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October 16, 2015

Mark Lipp 202.719.7503 mlipp@wileyrein.com

#### **VIA MESSENGER**

Marlene H. Dortch, Esq. Secretary Federal Communications Commission 445 12<sup>th</sup> Street, SW Washington, DC 20554 Accepted / Filed

Federal Communications Commission Office of the Secretary

OCT 16 2015

Attention: Media Bureau

Re: Application for Moment Method License and Direct Measurement of

Power on FCC Form 302-AM

Multicultural Radio Broadcasting Licensee, LLC Station KCHN(AM), Brookshire, Texas Facility Identifier Number 68124

Dear Ms. Dortch:

Transmitted herewith on behalf of Multicultural Radio Broadcasting Licensee, LLC ("MRBL"), the licensee of Station KCHN(AM) identified above, are an original and two copies of its application for license and direct measurement of power. MRBL's consulting engineer used the Method of Moments to prepare a proof-of-performance for the authorized and unmodified KCHN antenna radiation pattern, the results of which are submitted herewith.

Please note that the associated \$1,480.00 filing fees were paid using FCC Fee Filer and proof of payment is included as part of this submission.

If there are any questions about this Application, please contact undersigned counsel for Multicultural Radio Broadcasting Licensee, LLC.

Sincerely,

Enclosures

OCT 16 2015

Federal Communications Commission

On Office of the Secretary

# Agency Tracking ID:PGC2747600 Authorization Number:211064 Successful Authorization -- Date Paid: 10/16/15 FILE COPY ONLY!!

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68124	FCCForm302-AM

Electronic Form 159 Page 1 of 1



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# Accepted / Filed

Federal Communications Commission Washington, D. C. 20554

Approved by OMB 3060-0627 Expires 01/31/98 FOR FCC USE ONLY OCT 16 2015

Federal Communications Commission
Office of the Secretary

# FCC 302-AM APPLICATION FOR AM BROADCAST STATION LICENSE

(Please read instructions before filling out form.

FOR	COMMISSION USE ONLY	
FILE	NO. BMML-20151016AGJ	

SECTION I - APPLICANT FEE INFORMATION							
1. PAYOR NAME (Last, First, Middle Initial)							
Multicultural Radio Broadcasting Licensee, LLC							
MAILING ADDRESS (Line 1) (Maximum 35 characters) 27 William Street							
MAILING ADDRESS (Line 2) (Maximum 35 characters)  11th Floor							
CITY New York	STATE OR COUNTRY (if fo New York	reign address)	ZIP CODE 10005				
TELEPHONE NUMBER (include area code) 212.431.4300	CALL LETTERS KCHN(AM)	OTHER FCC IDE	NTIFIER (If applicable)				
2. A. Is a fee submitted with this application?		7.	✓ Yes No				
B. If No, indicate reason for fee exemption (see 47 C.F.R. Section							
Governmental Entity Noncommercial educ	ational licensee O	ther (Please explain)	):				
C. If res, provide the following information:							
Enter in Column (A) the correct Fee Type Code for the service you a Fee Filing Guide." Column (B) lists the Fee Multiple applicable for this	are applying for. Fee Type Cos application. Enter fee amou	odes may be found int due in Column (C	in the "Mass Media Services				
(A) (B)	(C)						
FEE TYPE FEE MULTIPLE	FEE DUE FOR FEE TYPE CODE IN COLUMN (A)		FOR FCC USE ONLY				
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To be used only when you are requesting concurrent actions which res	sult in a requirement to list mor	e than one Fee Type	e Code				
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ADD ALL AMOUNTS SHOWN IN COLUMN C, AND ENTER THE TOTAL HERE.	TOTAL AMOUNT REMITTED WITH TH APPLICATION	IS	FOR FCC USE ONLY				
THIS AMOUNT SHOULD EQUAL YOUR ENCLOSED REMITTANCE.	\$						

SECTION II - APPLICAN  1. NAME OF APPLICANT  Multicultural Radio Broadcas						
MAILING ADDRESS 27 William Street, 11th Floo	г	· · · · · · · · · · · · · · · · · · ·				
CITY New York			STATE New Y	′ork	ZIP CODE 10005	
2. This application is for:	Commercial AM Direct	ctional	☐ Noncomn	nercial Ion-Directional		
Call letters	Community of License	Construct	tion Permit File No.	Modification of Construction Permit File No(s).	Expiration Date of Last Construction Permit	
KCHN(AM)	Brookshire, TX		N/A	N/A	N/A	
3. Is the station no accordance with 47 C.F.  If No, explain in an Exhi		to auto	matic program	test authority in	Yes No	o
4. Have all the terms construction permit beer	s, conditions, and oblig n fully met?	ations s	et forth in the	above described	Yes No	0
If No, state exceptions in	n an Exhibit.				N/A	
the grant of the underl representation contained	ges already reported, ha ying construction permit d in the construction perr	which w	would result in a	any statement or	Yes No	D
If Yes, explain in an Exl	TIDIT.					
	ed its Ownership Report ce with 47 C.F.R. Sectior			ership	Yes No	
If No, explain in an Exhil	oit.				Does not apply  Exhibit No.	у
7. Has an adverse finding been made or an adverse final action been taken by any court or administrative body with respect to the applicant or parties to the application in a civil or criminal proceeding, brought under the provisions of any law relating to the following: any felony; mass media related antitrust or unfair competition; fraudulent statements to another governmental unit; or discrimination?						
involved, including an id (by dates and file numb information has been required by 47 U.S.C. So of that previous submiss the call letters of the sta	ttach as an Exhibit a fuentification of the court opers), and the disposition earlier disclosed in correction 1.65(c), the application by reference to the ation regarding which the filling; and (ii) the dispose	or adminion of the nection ant need file number application	strative body an litigation. Wh with another a only provide: (i) per in the case (ation or Section	d the proceeding ere the requisite application or as an identification of an application, 1.65 information	Exhibit No.	

8. Does the applicant, or any party to the application, have the expanded band (1605-1705 kHz) or a permit or license expanded band that is held in combination (pursuant to the 5 with the AM facility proposed to be modified herein?	either in the existing band or	Yes V No
If Yes, provide particulars as an Exhibit.		Exhibit No.
The APPLICANT hereby waives any claim to the use of any against the regulatory power of the United States becaus requests and authorization in accordance with this applicatio amended).	e use of the same, whether by	license or otherwise, and
The APPLICANT acknowledges that all the statements ma material representations and that all the exhibits are a materi		
CERTIFI	CATION	
1. By checking Yes, the applicant certifies, that, in the case or she is not subject to a denial of federal benefits that incl to Section 5301 of the Anti-Drug Abuse Act of 1988, 21 U case of a non-individual applicant (e.g., corporation, partner association), no party to the application is subject to a deincludes FCC benefits pursuant to that section. For the depurposes, see 47 C.F.R. Section 1.2002(b).	udes FCC benefits pursuant S.C. Section 862, or, in the ship or other unincorporated mial of federal benefits that	√ Yos No
<ol><li>I certify that the statements in this application are true, co and are made in good faith.</li></ol>	mplete, and correct to the best of	my knowledge and belief,
Name	Signature	100
Yvonne S. Liu	MIG	ILILLY
Title Secretary	Odic	.431.4300
WILLELL EALSE STATEMENTS ON THIS EODIN AR	E DHNISHARI E RV EINE AND	IOD IMPRISONMENT

WILLFUL FALSE STATEMENTS ON THIS FORM ARE PUNISHABLE BY FINE AND/OR IMPRISONMENT (U.S. CODE, TITLE 18, SECTION 1001), AND/OR REVOCATION OF ANY STATION LICENSE OR CONSTRUCTION

FCC NOTICE TO INDIVIDUALS REQUIRED BY THE PRIVACY ACT AND THE PAPERWORK REDUCTION ACT

The solicitation of personal information requested in this application is authorized by the Communications Act of 1934, as amended. The Commission will use the information provided in this form to determine whether grant of the application is in the public interest. In reaching that determination, or for law enforcement purposes, it may become necessary to refer personal information contained in this form to another government agency. In addition, all information provided in this form will be available for public inspection. If information requested on the form is not provided, the application may be returned without action having been taken upon it or its processing may be delayed white a request is made to provide the missing information. Your response is required to obtain the requested authorization.

Public reporting burden for this collection of information is estimated to average 639 hours and 53 minutes per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing the burden, can be sent to the Federal Communications Commission. Records Management Branch, Paperwork Reduction Project (3060-0627), Washington, D. C. 20554. Do NOT send completed forms to this address.

THE FOREGOING NOTICE IS REQUIRED BY THE PRIVACY ACT OF 1974, P.L. 93-579, DECEMBER 31, 1974, 5 U.S.C. 552a(e)(3), AND THE PAPERWORK REDUCTION ACT OF 1980, P.L. 96-511, DECEMBER 11, 1980, 44 U.S.C. 3507.

FCC 302-AM (Page 3) August 1995 HATFIELD & DAWSON

CONSULTING ELECTRICAL ENGINEERS 9500 GREENWOOD AVE. N. SEATTLE, WASHINGTON 98103

TELEPHONE (206) 783-9151 FACSIMILE (206) 789-9834 E-MAIL hatdaw@hatdaw.com

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BENJAMIN F. DAWSON III, PE

STEPHEN S. LOCKWOOD, PE

THOMAS M. ECKELS, PE

DAVID J. PINION, PE

ERIK C. SWANSON, PE

**ENGINEERING REPORT:** 

APPLICATION FOR LICENSE and Direct Power Measurement

RADIO STATION KCHN, Brookshire, TX 1050 kHz, 410 Watts, DA-D Facility ID #68124

October 14, 2015

# APPLICATION FOR LICENSE and Direct Power Measurement

#### RADIO STATION KCHN, Brookshire, TX 1050 kHz, 410 Watts, DA-D Facility ID #68124

#### Purpose of Application

Item 1	Tower Impedance Measurements and Verification of Method of Moments Model
Item 2	Derivation of Operating Parameters for Directional Antenna
Item 3	Method of Moments Model Details for Towers Driven Individually
Item 4	Method of Moments Model Details for Directional Antenna
Item 5	Array Geometry
Item 6	Sampling Line Measurements
Item 7	Reference Field Strength Measurements
Item 8	Direct Measurement of Power
Item 9	Antenna Monitor Data, Sample Device Measurements

Appendix A License BL-20010202ADZ (Most Recent Complete License Document)

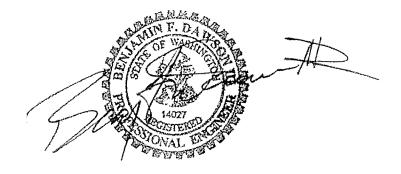
Appendix B FCC Form 302-AM

#### **Purpose of Application**

This engineering exhibit supports an application for a "moment method license" for the presently authorized and unmodified antenna radiation pattern of radio station KCHN, Brookshire, TX. KCHN is authorized per license to operate on 1050 kHz with a power of 410 Watts Daytime only, employing a directional antenna.

The antenna towers and ground system are unmodified from their established conditions and adjustments of the antenna parameters were made in accordance with the terms of the license and specifications provided for the previous licensing of the station. Information is provided herein demonstrating that the directional antenna parameters for the pattern authorized by the station license have been determined in accordance with the requirements of section 73.151(c) of the FCC Rules. The system has been adjusted to produce antenna monitor parameters within +/- 5 percent in ratio and +/- 3 degrees in phase of the modeled values, as required by the Rules. Measurements described in this report were made by George Schrank, George Butch, and by the undersigned.

Benjamin F. Dawson III, P.E.



October 14, 2015

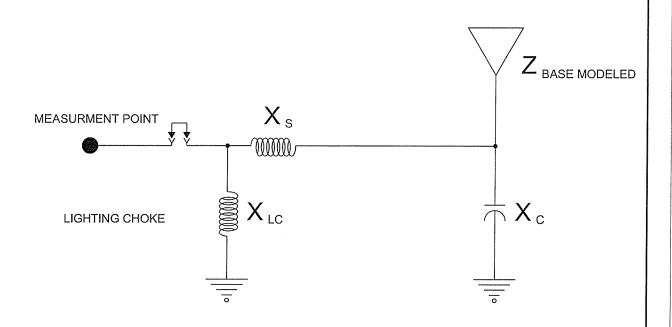
#### Item 1

#### Analysis of Tower Impedance Measurements to Verify Method of Moments Model

Tower impedance measurements were made at the locations of the sample system current transformers using an HP 8751A network analyzer in a calibrated measurement system. The other towers were open circuited at the same point where impedance measurements were made (the "reference points") for each of the measurements.

Circuit calculations were performed to relate the method of moments modeled impedances at the tower feed points to those at the current sample device locations as shown in the table. The base conditions shown for each tower, which includes the stray capacitances, were used in the moment method model as a load at ground level for the open circuited case. The static drain chokes in use have been included in the network for the tower being modeled despite their relatively high impedances. The long lead series inductances in the antenna tuning equipment buildings have been measured and those measured values, some of which are greater than 10  $\mu$ H, are used in those base region network models.

In addition to the page showing the schematic of the assumed circuit and tabulation of calculated values, a page with the result of calculations using the NETBW circuit analysis program is shown. These calculations show the impedance transformations and phase shifts between the tower base values produced by the MININEC moment method model and the location of the current sample devices used to produce the antenna monitor input signals.



TOWER	X <sub>LC</sub> (Ω)	*X <sub>s</sub> (Ω)	X <sub>C</sub> (Ω)	$Z_{\substack{BASE \\ MODELED}}(\Omega)$	Z <sub>MP</sub> (Ω) MODELED	Z <sub>MP</sub> (Ω) MEASURED
#1	+j2500	+j 57.4	-j10,000	24.35 -j53.74	24.01+j4.1	24.15+j4.55
#2	+j2500	+j 60.2	-j10,000	23.66 -j55.16	23.3+j5.49	23.55+j6.23
#3	+j2500	+j 71.7	-j10,000	23.61 -j55.2	23.04+j16.8	23.55+j16.6
#4	+j2500	+j 67.85	-j10,000	23.535 -j53.48	23.01+j14.7	22.88+j14.7

\* NOTE: LEAD INDUCTANCE VALUES ARE MEASURED PER 73.151 (c) (1) (vii) SINCE SOME EXCEED 10  $\mu H$ 

Dwayne Straume, H&D

9/1/2015

KCHN TABLE.dwg

HATFIELD & DAWSON CONSULTING ENGINEERS

ANALYSIS OF TOWER IMPEDANCE MEASUREMENTS TO VERIFY METHOD OF MOMENTS MODEL

RADIO STATION KCHN 1050 kHz

BROOKSHIRE, TX

9/2015

NETBW CALCULATION OF IMPEDANCE AT ATU OUTPUT (SAMPLE DEVICE/IMPEDANCE MEASUREMENT LOCATION) AS MODIFIED BY BASE CAPACITANCE, SERIES FEED PIPE INDUCTANCE AND STATIC DRAIN INDUCTOR

#### TOWER 1

FREQUENCY (KHZ)	LOAD RESISTANCE	LOAD REACTANCE	INPUT RESISTANCE	INPUT REACTANCE	PHASE SHIFT
1050.0	24.350	-53.740	24.0132	4.1139	+0.4125
TOWER 2					
FREQUENCY (KHZ)	LOAD RESISTANCE	LOAD REACTANCE	INPUT RESISTANCE	INPUT REACTANCE	PHASE SHIFT
1050.0	23.660	-55.160	23.3003	5.4940	+0.4003
TOWER 3					
FREQUENCY (KHZ)	LOAD RESISTANCE	LOAD REACTANCE	INPUT RESISTANCE	INPUT REACTANCE	PHASE SHIFT
1050.0	23.610	-55.190	23.0395	16.8603	+0.3971
TOWER 4					
FREQUENCY (KHZ)	LOAD RESISTANCE	LOAD REACTANCE	INPUT RESISTANCE	INPUT REACTANCE	PHASE SHIFT
1050.0	23.535	-53.480	23.0136	14.7283	+0.3964

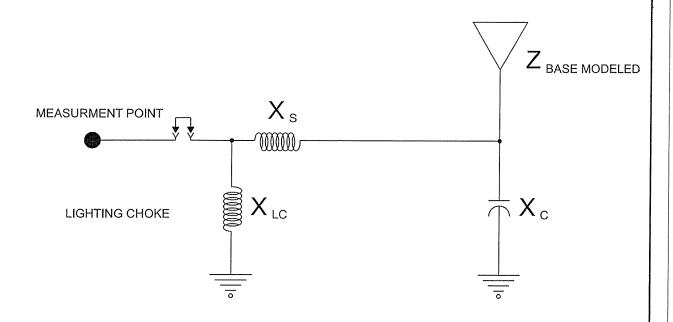
Item 2

Derivation of Operating Parameters for Directional Antenna - KCHN

The method of moments model of the array, following verification with the measured individual open circuited base impedances, was used for directional antenna calculations. Calculations were made to determine the complex voltage values for sources located at ground level at the base of each tower of the array to produce current moment sums for the towers that, when normalized, equated to the theoretical field parameters of the authorized directional antenna pattern. With these voltage sources, the tower currents and phases were calculated. 20 segments were used for towers in the moment method model. The currents and voltages at the tower bases (segments 1, 21, 41, and 61) were used to calculate the currents at the sample device locations by Kirchoff's law, using the analysis program NETBW.

Tower	Modeled Current Pulse	Base Current Magnitude	Base Current Phase	Antenna Monitor Sample Ratio	Antenna Monitor Sample Phase
1 W	1	2.2446	132.6	0.439	131.6
2 CW	21	5.084	1.1	1.0	0
3 CE	41	4.4781	226.2	0.889	-134.8
4 E*	61	1.5276	90.5	0.306	90.2

\* NOTE: Negative Tower!



TOWER	X <sub>LC</sub> (Ω)	*X <sub>S</sub> (Ω)	X <sub>C</sub> (Ω)	Z <sub>BASE</sub> (Ω)	Z <sub>MP</sub> (Ω)	CURRENT (Ω) PHASE ▲
#1	+j2500	+j 57.4	-j10,000	4.22 -j63.55	4.186-j5.75	+0.0717°
#2	+j2500	+j 60.2	-j10,000	11.32 -j51.67	11.12+j9.39	+0.1913°
#3	+j2500	+j 71.7	-j10,000	8.67 -j35.3	8.36+j36.02	+0.145°
#4	+j2500	+j 67.85	-j10,000	33.27 -j2.6	-31.58+j68.89	-0.552°

<sup>\*</sup> NOTE: MEASURED VALUES

Dwayne Straume, H&D

9/1/2015

KCHN TABLE,dwg

HATFIELD & DAWSON CONSULTING ENGINEERS

CALCULATION OF OPERATING ANTENNA MONITOR VALUES FROM MOMENT METHOD MODEL

RADIO STATION KCHN 1050 kHz

BROOKSHIRE, TX

9/2015

NETBW CALCULATIONS OF IMPEDANCE AT ATU OUTPUT (SAMPLE DEVICE/IMPEDANCE MEASUREMENT LOCATION) AS MODIFIED BY BASE CAPACITANCE, FEED PIPE SERIES INDUCTANCE, AND STATIC DRAIN INDUCTANCE

#### FOR DRIVEN RADIATION PATTERN

TOWER 1 FREQUENCY (KHZ)	LOAD RESISTANCE	LOAD REACTANCE	INPUT RESISTANCE	INPUT REACTANCE	PHASE SHIFT
1050.0	4.220	-63.550	4.1861	-5.7567	+0.0717
	LOAD RESISTANCE	LOAD REACTANCE	INPUT RESISTANCE	INPUT REACTANCE	PHASE SHIFT
1050.0	11.320	-51.070	11.1214	9.3915	+0.1913
TOWER 3 FREQUENCY (KHZ) 1050.0	LOAD RESISTANCE	LOAD REACTANCE 	INPUT RESISTANCE	INPUT REACTANCE	PHASE SHIFT +0.1450
TOWER 4 FREQUENCY (KHZ)	LOAD RESISTANCE	LOAD REACTANCE	INPUT RESISTANCE	INPUT REACTANCE	PHASE SHIFT
1050.0	-33.270	-2.600	-31.5796	63.8953	+0.5521

Item 3

Method of Moments Model Details for Towers Driven Individually - KCHN

The array of towers was modeled using MININEC. A single wire was used to represent each tower, which are uniform cross section. The top and bottom wire end points were specified using the theoretical directional antenna specifications in electrical degrees. The maximum and minimum segment lengths are 3.825 and 3.775 electrical degrees respectively.

Each tower's modeled height relative to its physical height falls within the required range of 75 to 125 percent and each modeled radius falls within the required range of 80 percent to 150 percent of the radius of a circle having a circumference equal to the sum of the widths of the tower sides. (Note that tower 4 has a larger face width than towers 1-3.

Tower #	Physical Height (degrees)	Modeled Height (degrees)	Modeled Percentage of Height	Modeled Radius (Meters)	Percent of Equivalent Radius
1 W	75.5	76.5	101.32	0.1819	125
2 CW	75.5	76.25	100.99	0.1819	125
3 CE	75.5	76.25	100.99	0.1819	125
4 E	75.5	75.5	100.00	0.262	120

The following pages show the details of the method of moments models for the individually driven towers.

# TOWER #1 DRIVEN WITH OTHER TOWERS LOADED WITH BASE REGION REACTANCE

H:\KCHN Brookshire\kchn1 08-28-2015 11:00:19

KCHN Brookshire, TX

#### GEOMETRY

Wire coordinates in degrees; other dimensions in meters Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.1819	20
		0	0	76.5		
2	none	82.2	112.	0	.1819	20
		82.2	112.	76.25		
3	none	164.4	111.6	0	.1819	20
		164.4	111.6	76.25		
4	none	246.8	111.8	0	.262	20
		246.8	111.8	75.5		

Number of wires = 4 current nodes = 80

	mini	mum	max	imum
Individual wires	wire	value	wire	value
segment length	4	3.775	1	3.825
radius	1	.1819	4	.262

#### ELECTRICAL DESCRIPTION

Frequencies (KHz)

_	frequency		no. of	segment length	(wavelengths)
no.	lowest	step	steps	minimum	maximum
1	1,050.	0	1	.0104861	.010625

#### Sources

source	node	sector	magnitude	phase	type
1	1	1	1.	Õ	võltage

#### Lumped loads

2000		resistance	reactance	inductance	capacitance	
passi load circu	node	(ohms)	(ohms)	(mH)	(uF)	
1	21	0	-10,000.	0	0	0
2	41	0	-10,000.	0	0	0
3	61	0	-10,000.	0	0	0

H:\KCHN Brookshire\kchn1 08-28-2015 11:00:19

#### IMPEDANCE

normalization = 50.

freq	resist	react	imped	phase	VSWR	S11	S12
(KHz)	(ohms)	(ohms)	(oĥms)	(deg)		dB	dΒ
source =	1; node	1, sector	r 1				
1,050.	24.346	-53.74	58.998	294.4	4.7003	-3.7532	-

# TOWER #2 DRIVEN WITH OTHER TOWERS LOADED WITH BASE REGION REACTANCE

H:\KCHN Brookshire\kchn2 08-28-2015 11:03:58

KCHN Brookshire, TX

#### GEOMETRY

Wire coordinates in degrees; other dimensions in meters Environment: perfect ground

wire 1	caps none	Distance 0	Angle 0	Z 0 76.5	radius .1819	segs 20
2	none	82.2	112.	0	.1819	20
3	none	82.2 164.4	112. 111.6	76.25 0	.1819	20
4	none	164.4 246.8	111.6 111.8	76.25 0	.262	20
		246.8	111.8	75.5		

Number of wires = 4 current nodes = 80

	mını	mum	max	imum
Individual wires	wire	value	wire	value
segment length	4	3.775	1	3.825
radius	1	.1819	4	.262

ELECTRICAL DE Frequencies frequencies no. lowest 1 1,050.	(KHz)	no. step 1		ıum	h (wavele maximum .010625	1
Sources source node 1 21	sector mag	gnitude	phase 0		type voltage	
Lumped loads	resistance	reactanc		uctance		
passive	resistance	reactance	e IIIa	uctance	capacita	.nce
load node circuit	(ohms)	(ohms)	(mH	<b>:</b> )	(uF)	
1 1 2 41 3 61	0 0 0	-10,000. -10,000. -10,000.	0 0 0		0 0 0	0 0 0
H:\KCHN Broo	kshire\kchn2	08-28-201	5 11:03	:58		
<pre>freq res (KHz) (oh source = 1;</pre>	tion = 50. ist react ms) (ohms) node 21, sect 659 -55.165	imped (ohms) or 1 60.025	phase (deg) 293.2	VSWR 4.9573	S11 dB -3.553	S12 dB -2.528

# TOWER #3 DRIVEN WITH OTHER TOWERS LOADED WITH BASE REGION REACTANCE

H:\KCHN Brookshire\kchn3 08-28-2015 11:06:40

KCHN Brookshire, TX

#### GEOMETRY

Wire coordinates in degrees; other dimensions in meters Environment: perfect ground

wire 1	caps none	Distance 0	Angle 0	Z 0 76.5	radius .1819	segs 20
2	none	82.2 82.2	112. 112.	76.3 0 76.25	.1819	20
3	none	164.4 164.4	111.6 111.6	0 76.25	.1819	20
4	none	246.8 246.8	111.8	0 75.5	.2725	20

Number of wires = 4 current nodes = 80

	minimum			maximum		
Individual wires	wire	value	wire	value		
segment length	4	3.775	1	3.825		
radius	1	.1819	4	.2725		

ELECTRICAL DESCRIPTION

no.	encies frequen lowest 1,050.		no. step 1	, - ,	um	h (wavele maximum .010625	l	
Source source 1	es e node 41		magnitude 1.	phase 0		type voltage		
	d loads	resistance	reactanc	e ind	uctance	capacita	ince	
passi load	node	(ohms)	(ohms)	(mH	)	(uF)		
circu: 1 2 3	1 21 61	0 0 0	-10,000. -10,000. -10,000.	0		0 0 0	0 0 0	
H:\KC	HN Broc	kshire\kchn	3 08-28-201	.5 11:06	:40			
no: freq (KHz) source								
	R #4 I TANCE	ORIVEN WIT	H OTHER TO	WERS LOA	DED WI	TH BASE	REGION	
H:\KC	HN Broo	okshire\kchn	4 08-28-201	.5 11:10	:09			
KCHN :	Brooksł	nire, TX						
GEOME Wire Envir	coordir	nates in deg : perfect gr	rees; other	dimension	s in met	ers		
wire 1	caps I	Distance D	Angle 0	Z 0		dius 819	segs 20	
2	none 8	32.2	0 112.	76.5 0 76.25	.1	819	20	
3	none 1	32.2 L64.4 L64.4	112. 111.6 111.6	76.25 0 76.25	. 1	819	20	
4	none 2		111.8 111.8 111.8	76.23 0 75.5	. 2	62	20	

ELECTRICAL DESCRIPTION Frequencies (KHz)

Number of wires

umber of wires = 4 current nodes = 80

minimum

Individual wires wire value wire value segment length 4 3.775 1 3.825 radius 1 .1819 4 .262

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maximum

no. l	requen owest ,050.	-	step 0		of ps	segme minim .0104	ıum	h (wavele maximum .010625	ı
Source source 1	_	sec 1	tor mag 1.	nitude		phase 0		type voltage	
Lumped	loads								
passiv	<b>a</b>	resis	tance	reactan	ce	ind	uctance	capacita	nce
load i	node	(ohms	)	(ohms)		(mH	)	(uF)	
1 2	1	0		-10,000		0		0	0
2 3	21 41	0		-10,000 -10,000		0 0		0	0
5	11	O		10,000	•	U		U	U
H:\KCHI	N Brool	kshire	\kchn4	08-28-20	15	11:10	:09		
	nalizat			. ,	,				
freq (KHz)	res: (ohr	ns)	react (ohms)	imped (ohms)		iase leg)	VSWR	S11 dB	S12 dB
source 1,050.	= 1;		61, sect -53.476	or 1 58.426	29	3.8	4.8178	-3.6589	-2.4461

Item 4

#### Method of Moments Model Details for Directional Antenna- KCHN

The array was modeled using MININEC with the individual tower characteristics that were verified by the respective tower impedance measurements. Calculations were made to determine the complex voltage values for sources located at ground level under each tower of the array to produce current moment sums for the towers that, when normalized, equated to the theoretical field parameters of the authorized directional antenna pattern. The following pages contain details of the method of moments model of the directional antenna pattern.

Tower	Wire	Base Node
1 W	1	1
2 CW	2	21
3 CE	3	41
4 E	4	61

#### MOMENT METHOD MODEL WITH DIRECTIONAL DRIVE VOLTAGES

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KCHN Brookshire, TX

#### GEOMETRY

Wire coordinates in degrees; other dimensions in meters Environment: perfect ground

wire		Distance	Angle	Z	radius	segs
1	none	0	0	0	.1819	20
0		0	0	76.5		
2	none	82.2	112.	0	.1819	20
2		82.2	112.	76.25		
3	none	164.4	111.6	0	.1819	20
		164.4	111.6	76.25		
4	none	246.8	111.8	0	.262	20
		246.8	111.8	75.5		

wires = 4 current nodes = 80 Number of wires

	mini	mum	maximum		
Individual wires	wire	value	wire	value	
segment length	4	3.775	1	3.825	
radius	1	.1819	4	.262	

#### ELECTRICAL DESCRIPTION

Frequencies (KHz)

r.r.edi	dencres (Vur)					
	frequency		no. o	f segment	length	(wavelengths)
no.	lowest	step	steps	minimum		maximum
1	1,050.	0	1	.0104861		.010625

# Sources

source	node	sector	magnitude	phase	type
1	1	1	202.168	46.4	võltage
2	21	1	376.062	283.6	voltage
3	41	1	230.164	150.	voltage
4	61	1	72.1065	275.	voltage

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#### TMPEDANCE

IMPEDANCE						
normalization :	= 50.					
freq resist (KHz) (ohms) source = 1; node	(ohms)	(oĥms)	phase (deg)	VSWR	S11 dB	S12 dB
1,050. 4.2181			273.8	31.053	55962	-9.1757
source = 2; node 1,050. 11.321			282.5	9.1403	-1.9082	-4.4908
source = 3; node 1,050. 8.6659			283.8	8.7033	-2.0049	-4.3209
source = 4; node 1,05033.272			184.5	***	***	***

#### C:\Users\Dawson\Desktop\kchndriven 08-25-2015 08:49:29

```
CURRENT rms
Frequency
              = 1050 \text{ KHz}
Input power = 410. watts
Efficiency
              = 100.
coordinates in degrees
                                                       phase
current
                                            maq
                                                               real
                                                                           imaginary
        X
                    γ
                                7
                                                       (deg)
no.
                                             (amps)
                                                                (amps)
                                                                            (amps)
                                                                -1.52041
GND
        0
                    0
                                0
                                            2.24466
                                                       132.6
                                                                           1.65131
 2
                    0
        0
                                3.825
                                            2.17829
                                                       132.5
                                                                -1.47246
                                                                           1.60524
 3
                    0
                                7.65
                                            2.12257
                                                       132.5
                                                                -1.43276
                                                                           1.56604
 4
                    0
                                11.475
        0
                                            2.06218
                                                       132.4
                                                                -1.39018
                                                                           1.52316
 5
                                            1.9954
                    0
                                                                -1.34346
        0
                                15.3
                                                       132.3
                                                                           1.47538
 6
                    0
                                19.125
        0
                                            1.92157
                                                       132.3
                                                                -1.29214
                                                                           1.42225
                                22.95
                                            1.84052
 7
        0
                    0
                                                       132.2
                                                                -1.23609
                                                                           1.36367
 8
                                26.775
                    0
                                                                           1.29963
        0
                                            1.75226
                                                       132.1
                                                                -1.17532
 9
                                30.6
        0
                    0
                                            1.65694
                                                       132.1
                                                                -1.10996
                                                                           1.23022
 10
        0
                    0
                                34.425
                                            1.55476
                                                       132.
                                                               -1.04014
                                                                           1.1556
 11
                    0
                                38.25
                                                       131.9
        0
                                            1.44599
                                                                -.966063
                                                                           1.07593
                                            1.33092
 12
        0
                    0
                                42.075
                                                       131.8
                                                               -.887949
                                                                           .991406
 13
        0
                    0
                                45.9
                                            1.20982
                                                       131.8
                                                               -.806009
                                                                           .902232
                                49.725
 14
        0
                    0
                                            1.083
                                                       131.7
                                                               -.720457
                                                                            .808597
 15
        0
                    0
                                53.55
                                            .950698
                                                       131.6
                                                               -.631493
                                                                            .710663
 16
                    0
                                57.375
                                            .813074
        0
                                                       131.5
                                                               -.539243
                                                                           .608529
 17
        0
                    0
                                                                           .502174
                                61.2
                                            .670136
                                                       131.5
                                                               -.443738
 18
        0
                    0
                                65.025
                                            .521556
                                                       131.4
                                                               -.344789
                                                                           .391332
 19
        0
                    0
                                68.85
                                            .366244
                                                       131.3
                                                               -.24171
                                                                           .275157
                                72.675
                                                       131.2
                                                               -.132512
 20
        0
                    0
                                            .201137
                                                                            .151317
END
                    0
                                76.5
                                            0
                                                       0
                                                               0
        -30.7927
-30.7927
GND
                    -76.2145
                                                               5.08304
                                                                           .0988019
                                0
                                            5.084
                                                       1.1
 22
                    -76.2145
                                3.8125
                                            4.96085
                                                               4.96032
                                                       .8
                                                                           .072098
 23
        -30.7927
                    -76.2145
                                7.625
                                            4.85182
                                                               4.85151
                                                                           .0547783
                                                       . 6
 24
        -30.7927
                    -76.2145
                                11.4375
                                            4.72908
                                                               4.72891
                                                       . 5
                                                                           .040108
 25
        -30.7927
                                                       .3
                    -76.2145
                                15.25
                                            4.58948
                                                               4.5894
                                                                           .0272788
        -30.7927
-30.7927
                    -76.2145
-76.2145
 26
                                19.0625
                                            4.43192
                                                       . 2
                                                               4.4319
                                                                           .0159554
 27
                                22.875
                                            4.25614
                                                       . 1
                                                               4.25613
                                                                           5.98E-03
                    -76.2145
 28
        -30.7927
                                26.6875
                                            4.06224
                                                       360.
                                                               4.06223
                                                                           -2.72E-03
        -30.7927
                    -76.2145
 29
                                30.5
                                            3.85057
                                                       359.8
                                                               3.85056
                                                                           -.0101799
        -30.7927
-30.7927
                    -76.2145
-76.2145
                                                       359.7
 30
                                            3.62162
                                34.3125
                                                               3.62159
                                                                           -.0164271
 31
                                38.125
                                            3.37599
                                                       359.6
                                                               3.37592
                                                                           -.0214629
                                41.9375
                                                       359.5
 32
        -30.7927
                    -76.2145
                                            3.1143
                                                               3.1142
                                                                           -.0252854
 33
        -30.7927
                    -76.2145
                                45.75
                                            2.8372
                                                       359.4
                                                               2.83707
                                                                           -.0278878
 34
        -30.7927
                    -76.2145
                                49.5625
                                            2.54533
                                                       359.3
                                                               2.54517
                                                                           -.0292599
        -30.7927
-30.7927
                    -76.2145
-76.2145
 35
                                                       359.2
                                                               2.23902
                                53.375
                                            2.23921
                                                                           -.0293879
                                57.1875
 36
                                            1.91918
                                                       359.2
                                                               1.91897
                                                                           -.0282529
 37
        -30.7927
                    -76.2145
                                                       359.1
                                61.
                                            1.58517
                                                               1.58496
                                                                           -.0258268
 38
        -30.7927
                                                       359.
                    -76.2145
                                64.8125
                                            1.23635
                                                               1.23616
                                                                           -.0220621
                                                       358.9
 39
        -30.7927
                    -76.2145
                                68.625
                                            .870067
                                                               .869904
                                                                           -.0168663
        -30.7927
 40
                    -76.2145
                                72.4375
                                            .478916
                                                       358.8
                                                               .478811
                                                                           -.0100278
        -30.7927
                    -76.2145
END
                                76.25
                                            0
                                                       n
                                                               0
                                                                           0
GND
        -60.5197
                    -152.855
                                            4.47808
                                                       226.2
                                                               -3.10049
                                                                           -3.23112
 42
        -60.5197
                    -152.855
                                3.8125
                                            4.39938
                                                       226.
                                                               -3.05778
                                                                           -3.16299
 43
        -60.5197
                    -152.855
                                7.625
                                            4.32184
                                                       225.8
                                                               -3.01135
                                                                           -3.10001
        -60.5197
                    -152.855
 44
                                            4.22858
                                11.4375
                                                       225.7
                                                               -2.95255
                                                                           -3.0271
        -60.5197
                                15.25
                                            4.11774
                                                      225.6
 45
                    -152.855
                                                               -2.88046
                                                                           -2.94257
 46
        -60.5197
                    -152.855
                                19.0625
                                            3.98876
                                                      225.5
                                                               -2.79486
                                                                           -2.84587
 47
        -60.5197
                    -152.855
                                22.875
                                            3.84158
                                                               -2.69579
                                                       225.4
                                                                           -2.73687
 48
        -60.5197
                    -152.855
                                26.6875
                                            3.67642
                                                       225.4
                                                               -2.58346
                                                                           -2.61569
```

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```
49
        -60.5197
                    -152.855
                               30.5
                                           3.49367
                                                     225.3
                                                             -2.45818
                                                                         -2.48256
                    -152.855
 50
        -60.5197
                               34.3125
                                           3.29381
                                                                         -2.33781
                                                     225.2
                                                             -2.32031
                                           3.07739
                                                     225.2
 51
        -60.5197
                    -152.855
                               38.125
                                                             -2.17024
                                                                         -2.18183
 52
                    -152.855
        -60.5197
                               41.9375
                                           2.84501
                                                     225.1
                                                             -2.00844
                                                                         -2.015
 53
        -60.5197
                    -152.855
                               45.75
                                           2.59726
                                                     225.
                                                             -1.83533
                                                                         -1.83775
 54
        -60.5197
                    -152.855
                               49.5625
                                           2.33473
                                                     225.
                                                             -1.65133
                                                                         -1.65048
 55
                    -152.855
        -60.5197
                               53.375
                                           2.05791
                                                     224.9
                                                             -1.4568
                                                                         -1.45351
 56
        -60.5197
                    -152.855
                               57.1875
                                           1.76708
                                                     224.9
                                                             -1.25196
                                                                         -1.24706
 57
        -60.5197
                    -152.855
                               61.
                                           1.4622
                                                     224.8
                                                             -1.03677
                                                                         -1.03108
                    -152.855
-152.855
 58
        -60.5197
                               64.8125
                                                     224.8
                                           1.14247
                                                             -.810683
                                                                         -.804998
 59
        -60.5197
                               68.625
                                           .805401
                                                     224.8
                                                             -.571925
                                                                         -.567074
 60
        -60.5197
                    -152.855
                               72.4375
                                                     224.7
                                                             -.315584
                                           .444093
                                                                         -.312451
END
        -60.5197
                    -152.855
                               76.25
                                           0
                                                             0
                                                     0
                    -229.15
        -91.6536
GND
                                           1.52764
                                                     90.5
                                                             -.0134418 1.52758
        -91.6536
                   -229.15
                               3.775
 62
                                           1.52178
                                                     91.4
                                                             -.0384121
                                                                        1.5213
        -91.6536
                    -229.15
                                           1.50874
                               7.55
                                                             -.0529901 1.50781
 63
                                                     92.
                   -229.15
 64
        -91.6536
                               11.325
                                           1.48789
                                                     92.5
                                                             -.06466
                                                                         1.48649
 65
                   -229.15
                                           1.45923
        -91.6536
                               15.1
                                                     92.9
                                                             -.0741564 1.45735
 66
        -91.6536
                   -229.15
                               18.875
                                           1.42281
                                                     93.3
                                                             -.0818101
                                                                        1.42046
 67
                   -229.15
                                                     93.7
        -91.6536
                               22.65
                                          1.37874
                                                             -.087776
                                                                         1.37594
                   -229.15
                                                     94.
 68
        -91.6536
                               26.425
                                           1.32715
                                                             -.0921339
                                                                        1.32395
                   -229.15
 69
        -91.6536
                               30.2
                                          1.26822
                                                     94.3
                                                             -.0949262
                                                                        1.26466
                               33.975
37.75
 70
        -91.6536
                   -229.15
                                          1.2021
                                                     94.6
                                                             -.0961757
                                                                        1.19825
 71
                   -229.15
        -91.6536
                                          1.12902
                                                     94.9
                                                             -.0958914
                                                                        1.12494
 72
        -91.6536
                   -229.15
                               41.525
                                          1.04917
                                                     95.1
                                                             -.0940777
                                                                        1.04495
 73
                   -229.15
                                                     95.4
        -91.6536
                               45.3
                                           .962767
                                                             -.0907295
                                                                        .958483
                               49.075
                                                                        .865739
 74
        -91.6536
                   -229.15
                                           .869984
                                                     95.7
                                                             -.0858392
 75
                   -229.15
        -91.6536
                               52.85
                                           .770977
                                                                         .766878
                                                     95.9
                                                             -.0793918
                   -229.15
 76
                                                             -.0713612
        -91.6536
                               56.625
                                           .665811
                                                     96.2
                                                                         .661976
 77
        -91.6536
                   -229.15
                               60.4
                                           .554404
                                                     96.4
                                                             -.0617027
                                                                        .55096
                   -229.15
 78
        -91.6536
                               64.175
                                           .436365
                                                     96.6
                                                             -.0503306
                                                                        .433453
                                                                        .308367
 79
        -91.6536
                   -229.15
                               67.95
                                           .310587
                                                     96.9
                                                             -.0370644
        -91.6536
                   -229.15
                               71.725
                                                     97.1
 80
                                           .174322
                                                             -.0215052
                                                                         .172991
END
        -91.6536
                   -229.15
                               75.5
                                                     0
```

# CURRENT MOMENT VALUES GENERATED FROM MININEC MODEL OF DRIVEN ARRAY

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CURRENT MOMENTS (amp-degrees) rms

Frequency = 1050 KHz Input power = 410. watts

			vertical cu	rrent moment
wire	magnitude	phase (deg)	magnitude	phase (deq)
1	114.975	132.1	114.975	132.1
2	265.531	360.	265.531	360.
3	240.04	225.4	240.04	225.4
4	85.7664	93.9	85.7664	93 9

Medium wave array vertical current moment (amps-degrees) rms (Calculation assumes tower wires are grouped together. The first wire of each group must contain the source.)

tower 1	magnitude 114.975	phase (deg) 132.1	normalized values
2	265.531	360.	1.0 / 0
3	240.04	225.4	0.904 / -134.6 (+225.4)
4	85.7664	93.9	0.323 / 93.9

#### Item 5

#### Array Geometry - KCHN

Per the provisions of the Commission's Public Notice DA 09-2340, October 29, 2009, paragraph 5, licensed stations applying to be re-licensed under the MM Docket 93-177 Rules are exempt from the requirement to submit an as-built surveyor's certification when there is no change in the theoretical patterns, as is the case in this application.

#### Item 6

#### Sampling System Measurements

Impedance measurements were made of the antenna monitor sampling system using a Hewlett Packard 8751A network analyzer in a calibrated measurement system. The measurements were made looking into the antenna monitor ends of the sampling lines for two conditions – with and without the sampling lines connected to the sampling transformers at the antenna tuning units.

The following table shows the frequency closest to the carrier frequency where series resonance – zero reactance corresponding with low resistance – was found. As frequencies of resonance occur at odd multiples of 90 degrees electrical length, the sampling line length at the resonant frequency below carrier frequency – which is the closest one to the carrier frequency – was found to be 90 electrical degrees. The electrical length at carrier frequency appearing in the table below was calculated by ratioing the carrier frequency to the resonant frequency.

Tower	Sampling Line Open-Circuited Resonance (kHz)	Sampling Line Electrical Length at 1050 kHz (Degrees)	1050 kHz Measured Impedance with Sample Transformer Connected
Tower 1	560.75	168.52	49.7 +J1.02
Tower 2	560.75	168.52	49.2 +J0.8
Tower 3	560.45	168.605	49.03 +J0.83
Tower 4	562.087	168.12	48.7 +J0.33

The sampling line lengths meet the requirement that they be equal in length within 1 electrical degree.

The characteristic impedance was calculated using the following formula, where R1 + jX1 and R2 + jX2 are the measured impedances of the +45 and -45 degree offset frequencies respectively:

$$Zo = ((R^2 + X^2)^{1/2} \times (R^2 + X^2)^{1/2})^{1/2}$$

Tower	-45° Offset	-45°	+45° Offset	+45°	Calculated
	Frequency	Measured	Frequency	Measured	Characteristic
	(kHz)	Impedance	(kHz)	Impedance	Impedance
		(Ohms)		(Ohms)	(Ohms)
1	280.375	0.1 -J50.04	841.125	4.7 +J49.42	50.09
2	280.375	0.84 -J50.45	841.125	4.95 +J49.79	50.25
3	280.225	0.8 -J50.116	840.675	4.7 +J49.35	49.74
4	280.0435	0.85 -J50.13	843.1305	4.7 +J49.57	49.96

The sampling line measured characteristic impedances meet the requirement that they be equal impedance within 2 Ohms.

#### Item 7

### **Reference Field Strength Measurements**

Reference field strength measurements were made along radials of three of the eight pattern inflection azimuths per inquiry and approval by the MB staff. The measured field strengths, point descriptions, and measured coordinates (NAD-83) are shown on the following page.

# REFERENCE POINT MEASUREMENTS KCHN BROOKSHIRE, TX

Date Description	10-Sep FM 529 - MP from last proof - N. side of road opp. mailboxes 10-Sep RC model airport - on ROW along W. side of prop. Between granset hirt & shed	10-Sep Addie Gee Rd MOR @ fence row5 mi. from FM 1887	10-Sep W. side of FM 159 - next to bridge rail	iu-Sep S. of Austin Branch Kd. @ Union Soldiers Cemetery marker		10-Sep Diemer Rd MP from last proof - MOR - bad null	10-Sep . 7 km S. of Vierick Rd between cotton fields	10-Sep int. of Peters-San Felipe & Grubbs Rd W. corner of yard between telco pedestal & water conn.	10-Sep E. side of SH 36 approx 100 feet S. of int.	10-Sep on FM 1094 - N. of driveway w/ double steel gate		12-Sep FM 359 - W. side of rd04 S. of bridge rail	12-Sep FM 362 - E. side of rd. @ telco pedestal	12-Sep FM 2855 - W. side of rd1 mi. S. of driveway to dump	12-Sep Lakecrest Manor Dr subdivision entrance - on grass esplanade	12-Sep Kingsland @ Westgreen - in parking lot driveway - approx 80 feet W. of Westgreen
Time	1415	1453	1506	761		1719	1632	1619	1608	1549		1429	1451	1511	1524	1555
mV/m	1.12	1.00	0.255			0.62	0.52	0.32	0.36	0.24		108.0	53.0	26.0	14.2	7.9
Long.	96° 3′1.30"W 96° 3′36.36"W	96° 4'42.83"W	96° 6'22.66"W	200		96° 5'15,95"W	96° 7'15.27"W	96° 9'18.37"W	96°10'13.82"W	96°13'38.07"W		96° 0'4.56"W	95°57'34.73"W	95°53'24.51"W	95°48'5.10"W	95°44'9.65"W
Lat.	29°54'53.95"N 29°56'19.62"N	29°59'2.12"N	30° 3'5,76"N 30° 6'37 03"N			29°51'51.04"N	29°51'15.72"N	29°50'39.26"N	29°50'22.83"N	29°49'22.23"N		29°52'3,44"N	29°51'11.94"N	29°49'45.75"N	29°47'55.51"N	29°46'34.05"N
340. 5 degrees	4.17 km 6.97 km	12.29 km	20.26 km 27.16 km		251.2 degrees	5.35 km	8.66 km	12.16 km	13.74 km	19.53 km	111.6 degrees	3.59 km	7.92 km	15.14 km	24.36 km	31.16 km

Measurements made by George Schank, who is experienced and qualified

in the use of the instrument for this purpose.

Calibration checked and within manufacturer's stated accuracy on Oct 14, 2015 against FIM-21 sn. 318, calibrated 6 Oct 2015

Measurement made using FIM-41 sn. 1274 calibrated 26 March 2001

#### Item 8

#### **Direct Measurement of Power - KCHN**

Common point impedance measurements were made with an HP-8751A network analyzer in a calibrated measurement system. The measurements were made at the phasor cabinet input adjacent to the common point current meter used to determine operating power. The impedance measured at this point was adjusted to a value of 50 ohms +/- j0 for the common point network. The licensed power is 410 watts, and with the 8% adjustment factor from 73.51(b)(1) the operating power is 443 watts, resulting in a common point current of 2.976 amperes, which has been rounded to 2.98 amperes on previous KCHN licenses.

Item 9

Antenna Monitor and Sampling System

The antenna monitor is a Potomac Instruments model AM-1901. The sample transformers are connected through equal lengths of Andrew 3/8 inch foam Heliax solid outer conductor transmission lines to the antenna monitor. The four sample lines are routed to the towers such that they are subject

to similar environmental conditions.

The antenna monitor was checked by placing the output of one of the tower monitoring circuits to the

antenna monitor inputs with a T connector. The three non-reference positions on the monitor read 0

degrees and a ratio of 1.000.

The sample transformers were tested with the configuration above, connecting the Tower 2 (reference

tower) sample transformer to the reference input of the monitor and alternately connecting the other

three transformers to a non-reference input. With the amplitude reference level being 1.000 and the

phase 0 degrees, the output levels and phases are as follows:

Transformer 1: 0.999 magnitude, phase +/- 0.0 degrees

Transformer 3: 0.999 magnitude, phase -0.1 degrees

Transformer 4: 0.999 magnitude, phase -0.3 degrees

All four transformers are Delta TCT-3 1.0 Volt/Amp devices. The manufacturer indicates these devices

have an absolute magnitude accuracy of ±2% and absolute phase accuracy of ±3 degrees. All of these

transformers have accuracies which exceed their factory specifications.

The serial numbers for the four transformers used in the KCHN sampling system are:

Tower 1: 16341; Tower 2: 17109; Tower 3: 17175; Tower 4: 17108

The sample transformers were then installed at the feed point in the antenna tuning units of their

respective towers.

Hatfield & Dawson Consulting Engineers



# United States of America FEDERAL COMMUNICATIONS COMMISSION

# AM BROADCAST STATION LICENSE

Authorizing Official:

Supervisory Engineer

Grant Date: June 06, 2001

This license expires 3:00 a.m.

local time, August 01, 2005.

Audio Division

Media Bureau

Official Mailing Address:

MULTICULTURAL RADIO BROADCASTING LICENSEE, LI Son Nguyen

27 WILLIAM STREET

11TH FLOOR

NEW YORK NY 10005

Facility Id: 68124

Call Sign: KCHN

License File Number: BL-20010202ADZ

License File Number: bu-20010202ADZ

This License Covers Permit No.: BP-19950912AA

Subject to the provisions of the Communications Act of 1934, subsequent acts and treaties, and all regulations heretofore or hereafter made by this Commission, and further subject to the conditions set forth in this license, the licensee is hereby authorized to use and operate the radio transmitting apparatus herein described.

This license is issued on the licensee's representation that the statements contained in licensee's application are true and that the undertakings therein contained so far as they are consistent herewith, will be carried out in good faith. The licensee shall, during the term of this license, render such broadcasting service as will serve the public interest, convenience, or necessity to the full extent of the privileges herein conferred.

This license shall not vest in the licensee any right to operate the station nor any right in the use of the frequency designated in the license beyond the term hereof, nor in any other manner than authorized herein. Neither the license nor the right granted hereunder shall be assigned or otherwise transferred in violation of the Communications Act of 1934. This license is subject to the right of use or control by the Government of the United States conferred by Section 606 of the Communications Act of 1934.

Hours of Operation: Daytime

Average hours of sunrise and sunset: Local Standard Time (Non-Advanced)

Jan.	7:15 AM	5:45 PM	Jul.	5:30 AM	7:30 PM
Feb.	7:00 AM	6:15 PM	Aug.	5:45 AM	7:00 PM
Mar.	6:30 AM	6:30 PM	Sep.	6:15 AM	6:30 PM
Apr.	6:00 AM	6:45 PM	Oct.	6:30 AM	6:00 PM
May	5:30 AM	7:15 PM	Nov.	6:45 AM	5:30 PM
Jun.	5:15 AM	7:30 PM	Dec.	7:15 AM	5:30 PM

Callsign: KCHN License No.: BL-20010202ADZ

Name of Licensee: MULTICULTURAL RADIO BROADCASTING LICENSEE, LLC

Station Location: BROOKSHIRE, TX

Frequency (kHz): 1050

Station Class: D

Antenna Coordinates:

Day

Latitude: N 29 Deg 52 Min 45 Sec Longitude: W 96 Deg 02 Min 08 Sec

Transmitter(s): Type Accepted. See Sections 73.1660, 73.1665 and

73.1670 of the Commission's Rules.

Nominal Power (kW): Day: 0.41

Antenna Input Power (kW): Day: 0.44

Antenna Mode: Day: DA

(DA=Directional Antenna, ND=Non-directional Antenna; CH=Critical Hours)

Current (amperes): Day: 2.98

Resistance (ohms): Day: 50

Antenna Registration Number(s):

Day:

Tower No. ASRN Overall Height (m)

1 1216804

2 1216805

3 1216807

4 1216808

Callsign: KCHN License No.: BL-20010202ADZ

DESCRIPTION OF DIRECTIONAL ANTENNA SYSTEM

Theoretical RMS (mV/m/km): Day: 209.7

Standard RMS (mV/m/km):

Augmented RMS (mV/m/km): Day:220.4

Q Factor:

Day:

#### Theoretical Parameters:

#### Day Directional Antenna:

Tower No.	Field Ratio	Phasing (Deg.)	Spacing (Deg.)	Orientation (Deg.)	Tower Ref Switch *	Height (Deg.)
1	0.4330	132.100	0.0000	0.000	0	75.5
2	1.0000	0.000	82.2000	112.000	0	75.5
3	0.9040	-134.600	164.4000	111.600	0	75.5
4	0.3230	93.900	246.8000	111.800	0	75.5

<sup>\*</sup> Tower Reference Switch

#### Augmentation Parameters:

Aug No.	Central Azimuth (Deg. T)	Span (Deg.)	Radiation at Central Azimuth (mV/m @ 1 km)
1	218.8	30.8	27.30

#### Day Directional Operation:

	Phase (Deg.)	Antenna Monitor Sample Current Ratio
1	132.2	0.432
2	0	1
3	-134.5	0.902
4	94	0.322

<sup>0 =</sup> Spacing and orientation from reference tower

<sup>1 =</sup> Spacing and orientation from previous tower

Antenna Monitor: POTOMAC INSTRUMENTS AM 1901

Sampling System Approved Under Section 73.68 of the Rules.

Monitoring Points:

Day Operation:

Radial (Deg. T)	Distance From Transmitter Maximum $(kM)$	Field Strength (mV/m)
4.7	4.2	5.37
17.5	4.25	3.16
203.4	4.08	3.2
251.2	5.35	1.98
307.3	3.9	3.69
340.5	4.16	1.8

Special operating conditions or restrictions:

- 1 The permittee/licensee in coordination with other users of the site must reduce power or cease operation as necessary to protect persons having access to the site, tower or antenna from radiofrequency electromagnetic fields in excess of FCC guidelines.
- 2 Monitor Point #1: is on the left (north) side of Crump Ferry Road in line with a large tree with a "Y" in the trunk, also on the north side of the street.

Monitor Point #2: is on the right (southwest) side of Route 359 opposite power pole No. 75773, which is on the northeast side of road. Monitor Point #3: is on the left(south) side of Garrett Road opposite cable pedestal No. 14-32R-10-1, which is on the north side of road. Monitor Point #4: is on the right (east) side of Diemer Road centered between the double access gates leading to the field.

Monitor Point #5: is approximately 0.1 miles north of the bend, on the right (east) side of Sunny Side Road in line with the fence, which is

right (east) side of Sunny Side Road in line with the fence, which is on the west side of road.

Monitor Point #6 is on the right (north) side of Crump Ferry Road opposite mailboxes 101R and 101W, which are on the south side of the road.

\*\*\* END OF AUTHORIZATION \*\*\*

J.		LICATION ENGI	NEERING DATA							
Name of Applicar										
	MULTICULTURAL RADIO BROADCASTING LICENSEE, LLC									
PURPOSE OF A	PURPOSE OF AUTHORIZATION APPLIED FOR: (check one)									
X s	Station License	е	X Direct Mea	asurement of Po	ower					
1. Facilities auth	1									
Call Sign		onstruction Permit	Frequency	Hours of Ope	eration		kilowatts			
KCHN	(if applicable NOT APPL		(kHz) 1050	DAYTIME		Night DNA	Day 0.410			
2. Station locatio	2. Station location									
State				City or Town	ı					
TEXAS				BROOKSHII	RE					
3. Transmitter loc	cation									
State	County			City or Town		Street address	-4: \			
TEXAS	WALI	LER		NR. PATT	ISON	(or other identification 9807 S. BUL				
4. Main studio lo	cation									
State	County			City or Town		Street address	ation)			
TEXAS	HARF	RIS		HOUSTON		(or other identification (or other identification (or other identification) (or other identifica	•			
5. Remote contro	ol point location	n (specify only if au	thorized direction	al antenna)						
State	County			City or Town		Street address	<i>(</i> :)			
TEXAS	HARI	RIS		HOUSTON		(or other identification 1782 W Sam	•			
6. Has type-approved stereo generating equipment been installed?  7. Does the sampling system meet the requirements of 47 C.F.R. Section 73.68?  X Yes No  Not Applicable  Attach as an Exhibit a detailed description of the sampling system as installed.  Exhibit No.  ENG. RPT.										
<ol><li>Operating cons</li><li>RF common point</li></ol>		ırrent (in amperes)	without	RF common	noint or antenna o	current (in amperes	:) without			
modulation for nig	ht system			modulation fo	r day system	98 A.	y without			
Measured antenna operating frequency Night		point resistance (in	ohms) at	Measured and operating free Night		point reactance (in	n ohms) at			
NONE		50.0 OF	HMS	NONE		, +/- J	0			
Antenna indication	ns for direction			J						
Tower	s	Antenna n Phase reading(s			onitor sample t ratio(s)	Antenna ba	se currents			
		Night	Day	Night	Day	Night	Day			
1 W		NO	131.6	NO	0.439	NO	NO			
2 CW	2 CW         NIGHT         0         NIGHT         1.0         NIGHT         LONGER           3 CE         OPER-         -134.8         OPER-         0.889         OPER-         REQUIRED									
4 E		ATION	90.2	ATION	0.306	ATION	REQUIRED			
Manufacturer and	type of antenr	na monitor: POTOI	MAC INSTRUME	ENTS AM-19	01					

#### SECTION III - Page 2

Description of antenr the array. Use separate	na system ((f directional anter sheets if necessary.)	nna is used, th	e information re	equested below shou	ld be given	for each element o		
Type Radiator UNIFORM CROSS SECTION GUYED VERTICAL TOWERS	NIFORM CROSS radiator above base above base, if obs		neight in meters round (without obstruction lighting)  Overall height in metabove ground (included obstruction lighting)			antenna is either top aded or sectionalized, escribe fully in an xhibit.		
·	60.0	61.0(1,3	)60.7(2,4)	NOT LIGHTE	ID D	Exhibit No. DNA		
Excitation	X Series	Shunt						
Geographic coordinates tower location.	to nearest second. For direct	lional antenna	give coordinate	es of center of array.	For single v	vertical radiator give		
North Latitude 29	52	45	West Longitud	le 0 96	02	08		
If not fully described abo	ve, attach as an Exhibit furth er and associated isolation ci	ner details and rcuits.	dimensions inc	cluding any other		Exhibit No. NONE		
Also, if necessary for a dimensions of ground sys	complete description, attac stem.	h as an Exhil	oit a sketch of	the details and		Exhibit No. ON FILE		
10. In what respect, if ar permit?	y, does the apparatus constr	ucted differ fro	m that describe	ed in the application fo	or construc	tion permit or in the		
NONE TOWER REGIS TOWERS NOT	TRATIONS: 1216804, LIGHTED OR PAINTED	1216805,	1216807, 1	L216808				
11. Give reasons for the	change in antenna or commo	n point resista	nce.					
NO CHANGE: ACU GROUNDI	SYSTEM RETUNED TO I	MM CALCULA IMPROVED	TED VALUES	3				
I certify that I represent tinformation and that it is to	he applicant in the capacity rue to the best of my knowled	indicated belonge and belief.	w and that I ha	ive examined the for	egoing stat	ement of technical		
Name (Please Print or Ty	•	S	gnature (check	appropriate box belo	)w) 🗸	/		
BENJ. F. DAWSON			I hay feraunt					
Address (include ZIP Cod	•		Date					
9500 GREENWOOD		}-		R 14, 2015				
SEATTLE, WA 981	.03 USA	Į le	Telephone No. (Include Area Code) 206 783 9151					
Technical Director		X	Registered	Professional Enginee	er			
Chief Operator	Chief Operator Technical Consultant							

Other (specify) CONSULTING ENGINEER