



1776 K STREET NW WASHINGTON, DC 20006 PHONE 202.719.7000 FAX 202.719.7049

7925 JONES BRANCH DRIVE McLEAN, VA 22102 PHONE 703.905.2800 FAX 703.905.2820

www.wileyrein.com



STAMP & RETURN

US BANK/FCC FEB 0 1 2011

Mark Lipp 202.719.7503 mlipp@wileyrei n.com

BY HAND DELIVERY

January 31, 2011

Federal Communications Commission c/o U.S. Bank - Government Lockbox #979089 SL-MO-C2-GL 1005 Convention Plaza St. Louis, MO 63101

Re:

Application for AM Broadcast Station License/

Request for Program Test Authority

Susquehanna Radio Corp.

Station KTCK(AM), Dallas, Texas Facility Identifier Number 8773 File Number BP-20091116ADS

Dear Ms. Dortch:

Transmitted herewith on behalf of Susquehanna Radio Corp., the licensee of Station KTCK(AM), are an original and two copies of its application for an AM broadcast station license to cover the construction authorized in construction permit BP-20091116ADS. This Permit authorizes operation on 1310 kHz with 25 kW of power during the day and 5 kW at night using directional antenna systems. The Technical Statement and Exhibits, prepared by R. Stuart Graham, include all of the technical details and show that the operating parameters of the daytime and nighttime directional antenna patterns were determined in compliance with Section 73.151(c) of the Commission's Rules.

If there are any questions about this Application, please contact undersigned counsel

Sincerely,

ML/dmk

Enclosure

13239132.1



1776 K STREET NW WASHINGTON, DC 20006 PHONE 202.719.7000 FAX 202.719.7049

7925 JONES BRANCH DRIVE McLEAN, VA 22102 PHONE 703.905.2800 FAX 703.905.2820

www.wileyrein.com



STAMP & RETURN Ams

US BANK/FCC FEB 0 1 2011

Mark Lipp 202.719.7503 mlipp@wileyrein.com

BY HAND DELIVERY

January 31, 2011

Federal Communications Commission c/o U.S. Bank – Government Lockbox #979089 SL-MO-C2-GL 1005 Convention Plaza St. Louis, MO 63101

Re: Application for AM Broadcast Station License/ Request for Program Test Authority Susquehanna Radio Corp. Station KTCK(AM), Dallas, Texas Facility Identifier Number 8773 File Number BP-20091116ADS

Dear Ms. Dortch:

Transmitted herewith on behalf of Susquehanna Radio Corp., the licensee of Station KTCK(AM), are an original and two copies of its application for an AM broadcast station license to cover the construction authorized in construction permit BP-20091116ADS. This Permit authorizes operation on 1310 kHz with 25 kW of power during the day and 5 kW at night using directional antenna systems. The Technical Statement and Exhibits, prepared by R. Stuart Graham, include all of the technical details and show that the operating parameters of the daytime and nighttime directional antenna patterns were determined in compliance with Section 73.151(c) of the Commission's Rules.

If there are any questions about this Application, please contact undersigned counsel for Susquehanna Radio Corp.

Sincerely,

ML/dmk

Enclosure

13239132 1

Federal Communications Commission Washington, D. C. 20554

Approved by OMB 3060-0627 Expires 01/31/98

FCC 302-AM APPLICATION FOR AM BROADCAST STATION LICENSE

(Please read instructions before filling out form.

FOR FCC USE ONLY	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	CES DIVISION
	700	

FOR COMMISSION USE ONLY
FILE N BAML- 2011 020 AFX

SECTION I APPLICANT FOR		MINL LOI	1020/AI-X
SECTION I - APPLICANT FEE INFORMATION 1. PAYOR NAME (Last, First, Middle Initial)			.0
Susquehanna Radio Corp.			
MAILING ADDRESS (Line 1) (Maximum 35 characters) 3280 Peachtree Road, NW, Suite 2300			
MAILING ADDRESS (Line 2) (Maximum 35 characters)			
CITY Atlanta	STATE OR COUNTRY (%)		
TELEPHONE NUMBER (include area code)	STATE OR COUNTRY (if for Georgia	oreign address)	ZIP CODE 30305
404.349.0700	CALL LETTERS	OTHER FCC IDE	NTIFIER (If applicable)
2. A. Is a fee submitted with this application?	KTCK(AM)	8773	
B. If No, indicate reason for fee exemption (see 47 C.F.R. Section	1		✓ Yes No
Governmental Entitle			
Thoricommercial educ	cational licensee O	ther (Please explain):
C. If Yes, provide the following information:	3254562		
-IIIEI IN COllimn (A) the serve to			
Enter in Column (A) the correct Fee Type Code for the service you a Fee Filing Guide." Column (B) lists the Fee Multiple applicable for this	is application. Enter fee amoun	des may be found i	n the "Mass Media Services
	8 2 000	it dae in Column (C).
(A) (B)	(C)		
FEE TYPE FEE MULTIPLE	FEE DUE FOR FEE		
M M R 0 0 0 1	TYPE CODE IN COLUMN (A)		FOR FCC USE ONLY
0 0 0	\$ 615.00		
be used only when you are requesting concurrent actions which rest (A)	ult in a nami		
(A) (B)		than one Fee Type	Code.
M O R 0 0 0 1	(C)	_ [OD 500 HOT
0 0 1	\$ 705.00		OR FCC USE ONLY
DD ALL AMOUNTS SHOWN IN COLUMN C,	TOTAL ANGLE		
- VIII VINIOUNIO SHOWN IN COLLIMALO	TOTAL AMOUNT		
D LINIER THE TOTAL HERE	REMITTED WITH THIS	Fo	OR ECC LISE ONLY
ID ENTER THE TOTAL HERE. IIS AMOUNT SHOULD EQUAL YOUR ENCLOSED MITTANCE.	\$ 1,320.00	FC	OR FCC USE ONLY

SECTION II - APPLICA 1. NAME OF APPLICANT	NT INFORMATION				
Susquehanna Radiio Cor	р.				
MAILING ADDRESS 3280 Peachtree Road, NV	V, Suite 2300				
CITY Atlanta			STATE Geor	gia	ZIP CODE
2. This application is for	: Commercial AM Direct	[ctional	Noncomi	mercial Non-Directional	30305
Call letters KTCK(AM)	Community of License Dallas, TX	ĺ	on Permit File No.	Modification of Construct Permit File No(s).	Expiration Date of Last Construction Permit 3/11/2013
 Is the station neaccordance with 47 C.F If No, explain in an Exhibit 		to auton	natic program	test authority in	Yes ✓ No Exhibit No. A
If No, state exceptions in	an Exhibit.				✓ Yes No Exhibit No.
 Apart from the chang the grant of the underly representation contained If Yes, explain in an Exh 	in the construction permit				Yes ✓ No Exhibit No.
6. Has the permittee file certification in accordance	d its Ownership Report (Fe with 47 C.F.R. Section 7	FCC Form 73.3615(b	n 323) or owner o)?	ship	Yes No
If No, explain in an Exhibi	t.				Does not apply Exhibit No.
7. Has an adverse finding or administrative body with criminal proceeding, brough felony; mass media relation another governmental unit	ght under the provisions of the antitrust or unfair of the antitrust or unfair of the antitrust of the antit	t or partie	s to the applica	ition in a civil or	Yes ✓ No
If the answer is Yes, attainvolved, including an ider (by dates and file number information has been earequired by 47 U.S.C. Sectof that previous submission the call letters of the static was filed, and the date of file	ris), and the disposition of a rise, and the disposition of a rise disclosed in connection 1.65(c), the applicant in by reference to the file on regarding which the contraction of the file of the fi	of the liti- ection with t need on number	ative body and gation. Wher hanother apply provide: (i) a in the case of	the proceeding e the requisite plication or as in identification an application,	Exhibit No.

8. Does the applicant, or any party to the application, have a the expanded band (1605-1705 kHz) or a permit or license expanded band that is held in combination (pursuant to the 5 with the AM facility proposed to be modified herein?	either in the existing band	or
If Yes, provide particulars as an Exhibit.	÷	Exhibit No.
The APPLICANT hereby waives any claim to the use of any against the regulatory power of the United States because requests and authorization in accordance with this application amended).	use of the same, wheth	ner by license or otherwise, and
The APPLICANT acknowledges that all the statements maderial representations and that all the exhibits are a material	de in this application and al part hereof and are incor	attached exhibits are considered porated herein as set out in full in
CERTIFIC	CATION	
1. By checking Yes, the applicant certifies, that, in the case or she is not subject to a denial of federal benefits that incluto Section 5301 of the Anti-Drug Abuse Act of 1988, 21 U. case of a non-individual applicant (e.g., corporation, partners association), no party to the application is subject to a de includes FCC benefits pursuant to that section. For the del purposes, see 47 C.F.R. Section 1.2002(b).	udes FCC benefits pursual S.C. Section 862, or, in the ship or other unincorporate nial of federal benefits the finition of a "party" for thes	nt de d at ee
I certify that the statements in this application are true, co and are made in good faith.	mplete, and correct to the	best of my knowledge and belief,
Name	Signature	
Richard S. Denning	Behord S_	Denning
THIS VP, Secretary and General Counsel	Date 1/31/11	Telephone Number 404.949.0700
WILLELL EALSE STATEMENTS ON THIS EODM AD	E BIINIQUADI E DV EINI	AND OD IMPRICANTENT

WILLFUL FALSE STATEMENTS ON THIS FORM ARE PUNISHABLE BY FINE AND/OR IMPRISONMENT (U.S. CODE, TITLE 18, SECTION 1001), AND/OR REVOCATION OF ANY STATION LICENSE OR CONSTRUCTION

FCC NOTICE TO INDIVIDUALS REQUIRED BY THE PRIVACY ACT AND THE PAPERWORK REDUCTION ACT

The solicitation of personal information requested in this application is authorized by the Communications Act of 1934, as amended. The Commission will use the information provided in this form to determine whether grant of the application is in the public interest. In reaching that determination, or for law enforcement purposes, it may become necessary to refer personal information contained in this form to another government agency. In addition, all information provided in this form will be available for public inspection. If information requested on the form is not provided, the application may be returned without action having been taken upon it or its processing may be delayed while a request is made to provide the missing information. Your response is required to obtain the requested authorization.

Public reporting burden for this collection of information is estimated to average 639 hours and 53 minutes per response, including the time for reviewing instructions, searching existing data cources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing the burden, can be sent to the Federal Communications Commission, Records Management Branch, Paperwork Reduction Project (3060-0627), Washington, D. C. 20554. Do NOT send completed forms to this address.

THE FOREGOING NOTICE IS REQUIRED BY THE PRIVACY ACT OF 1974, P.L. 93-579, DECEMBER 31, 1974, 5 U.S.C. 552a(e)(3), AND THE PAPERWORK REDUCTION ACT OF 1980, P.L. 98-511, DECEMBER 11, 1980, 44 U.S.C. 3507.

Exhibit A

The construction permit BP-20091116ADS which authorized an increase in the directional daytime power of Station KTCK(AM) from 9 to 25 kiloWatts contains Special Operting Condition #1 which requires a complete proof-of-performance of the daytime directional antenna system. This proof-of-performance must be evaluated before Program Test Authority is approved. As a result, KTCK(AM) is not eligible for automatic Program Test Authority. It should be noted that the licensed nighttime directional operation did not change.

	ant	PLICATION ENG		<u> </u>			
Susquehanna		rp.	•				
		TION APPLIED F	OR: (check and	1			
~ ~	Station Licer						
				ct Measurement	of Power		
1. Facilities auth	norized in co	nstruction permit					
-	(if applicat	f Construction Pe		Hours	of Operation	D.	
KTCK	BP-2009	ble) 1116ADS	(kHz) 1310			i Night	in kilowatts Day
2. Station location	on				U	5.0	25.0
State				City or T	Oun		
Texas				1			
3. Transmitter los	cation			Dallas			
State	County	-					
Texas	Dallas			City or T		Street address	
4. Main studio loc				Coddel	1	(or other identification 900 E. Ledber	cation)
01-4	County					1 v v D. Deabe	uer Dr.
an l	•			City or To	own	Street address	
	Dallas			Dallas		(or other identific	ation)
5. Remote control State	County location	on (specify only it	authorized direct	ctional antenna)		13300 Maple A	ve., Suite 1310
	County			City or To		Street address	
Texas	Dallas			Dallas		(or other identific	ation)
						3500 Maple A	ve, Suite 1310
 Has type-approv Does the sampli 					?	☐ Yes ※ Yes	⊠ No □ No
				•		☐ Not	Annlicable
Attach as an Exhibit a detailed description of the sampling system as installed. Not Applicable							
do an Ext	Gottant						
			he sampling sys	tem as installed	l.		
Operating consta	ents:			item as installed	l. 	Exhibit 6	
Operating consta F common point or odulation for night	ants:			RF commo	n point or antonno	6	No.
Operating consta F common point or odulation for night 6.82	ants: antenna cui system	rrent (in amperes) without	RF common			No.
Operating consta F common point or odulation for night s 6.82 easured antenna or	ants: antenna cui system	rrent (in amperes) without	RF common modulation 23.0	n point or antenna for day system	a current (in amperes	No.) without
Operating consta F common point or odulation for night	ants: antenna cui system	rrent (in amperes) Dint resistance (in) without	RF common modulation 23.0	n point or antenna for day system	6	No.) without
Operating consta F common point or odulation for night: 6.82 easured antenna or perating frequency	ants: antenna cui system	rrent (in amperes) Dint resistance (in Day) without	RF common modulation 23.0 Measured a operating from Night	n point or antenna for day system	a current (in amperes	No.) without
Operating consta F common point or codulation for night s 6.82 easured antenna or perating frequency ght 49.5	ants: rantenna cur system r common po	oint resistance (in Day 49.7) without	RF common modulation 23.0 Measured a operating from	n point or antenna for day system	a current (in amperes on point reactance (in	No.) without
Operating consta F common point or odulation for night: 6.82 easured antenna or perating frequency ght 49.5 tenna indications for	ants: rantenna cur system r common po	oint resistance (in Day 49.7 I operation) without ohms) at	RF common modulation 23.0 Measured a operating from Night +1.7	n point or antenna for day system intenna or commo equency	a current (in amperes	No.) without
Operating consta F common point or codulation for night s 6.82 easured antenna or perating frequency ght 49.5	ants: rantenna cur system r common po	oint resistance (in Day 49.7 I operation Antenna) without ohms) at	RF common modulation 23.0 Measured a operating from Night +1.7	n point or antenna for day system intenna or commo equency	a current (in amperes on point reactance (in Day +1.0) without ohms) at
Operating consta F common point or odulation for night s 6.82 easured antenna or perating frequency ght 49.5 tenna indications for	ants: rantenna cur system r common po	oint resistance (in Day 49.7 I operation Antenna Phase reading Night	ohms) at monitor (s) in degrees	RF common modulation 23.0 Measured a operating from Night +1.7 Antenna macurrer	n point or antenna for day system intenna or commo equency	a current (in amperes on point reactance (in Day +1.0 Antenna bas) without ohms) at
Operating consta F common point or odulation for night: 6.82 easured antenna or perating frequency ght 49.5 tenna indications for Towers NE) CE	ants: rantenna cur system r common po	oint resistance (in Day 49.7 I operation Antenna Phase reading Night	ohms) at monitor (s) in degrees Day 0.00	RF common modulation 23.0 Measured a operating from Night +1.7 Antenna macurrer Night	n point or antenna for day system intenna or commo equency	a current (in amperes on point reactance (in Day +1.0) without ohms) at
Operating consta F common point or odulation for night s 6.82 easured antenna or perating frequency ght 49.5 tenna indications for Towers (NE) (CE) (SE)	ants: rantenna cur system r common po	prient (in amperes) Day 49.7 Loperation Antenna Phase reading Night 114.00	monitor (s) in degrees Day 0.00	RF common modulation 23.0 Measured a operating from Night +1.7 Antenna macurrer Night 0.770	n point or antenna for day system Intenna or commo equency Inonitor sample nt ratio(s) Day 1.000 0.968	a current (in amperes on point reactance (in Day +1.0 Antenna bas	No.) without Ohms) at
Operating consta F common point or odulation for night: 6.82 easured antenna or perating frequency ght 49.5 tenna indications for Towers NE) CE	ants: rantenna cui system r common po	prient (in amperes) Day 49.7 Loperation Antenna Phase reading Night 114.00 0.00	monitor (s) in degrees Day 0.00 73.1	RF common modulation 23.0 Measured a operating from Night +1.7 Antenna macurrer Night 0.770 1.000	n point or antenna for day system Intenna or commo equency Inonitor sample nt ratio(s) Day 1.000 0.968 0.879	a current (in amperes on point reactance (in Day +1.0 Antenna bas	No.) without Ohms) at
Operating consta F common point or odulation for night s 6.82 easured antenna or perating frequency ght 49.5 tenna indications for Towers (NE) (CE) (SE)	ants: rantenna cui system r common po	prient (in amperes) Day 49.7 Loperation Antenna Phase reading Night 114.00 0.00	monitor (s) in degrees Day 0.00	RF common modulation 23.0 Measured a operating from Night +1.7 Antenna macurrer Night 0.770	n point or antenna for day system Intenna or commo equency Inonitor sample nt ratio(s) Day 1.000 0.968	a current (in amperes on point reactance (in Day +1.0 Antenna bas	No.) without ohms) at
Operating consta F common point or odulation for night s 6.82 easured antenna or perating frequency ght 49.5 tenna indications for Towers (NE) (CE) (SE)	ants: rantenna cur system r common po	oint resistance (in Day 49.7 I operation Antenna Phase reading Night 114.00 0.00 -62.9	monitor (s) in degrees Day 0.00 73.1 -61.2	RF common modulation 23.0 Measured a operating from Night +1.7 Antenna magnetic courrer Night	n point or antenna for day system Intenna or commo equency Inonitor sample nt ratio(s) Day 1.000 0.968 0.879	a current (in amperes on point reactance (in Day +1.0 Antenna bas	No.) without ohms) at

SECTION III - Page 2

9. Description of antenna system (If directional antenna is used, the information requested below should be given for each element of the array. Use separate sheets if necessary.)

Type Radiator ,	Overall height in meters of radiator above base insulator, or above base,	Overall heigh above ground obstruction lig	l (without		ght in meters ind (include	If antenna is either top loaded or sectionalized, describe fully in an Exhibit.
Uniform cross-	if grounded.		Jg/		99/	
section, guyed steel towers	143.3	145.1		146.0	1	Exhibit No.
Steel towers	143.3	143.1				
Excitation	🖔 Series	Shunt		1046214 1046215	1046216 1046217	
Geographic coordinates tower location.	to nearest second. For direct	ional antenna	give coordinate	s of center	of array. For sing	gle vertical radiator give
North Latitude 32	. 56 '	41 "	West Longitu	de 96°	56	25
	ove, attach as an Exhibit furt er and associated isolation ci		dimensions in	cluding any	other	Exhibit No.
Also, if necessary for a co of ground system.	mplete description, attach as a	an Exhibit á ske	etch of the detail	s and dimer	nsions	Exhibit No.
10. In what respect, if an permit? None	ny, does the apparatus constr	ructed differ fro	m that describe	ed in the ap	plication for cons	truction permit or in the
11. Give reasons for the N/A	change in antenna or commo	on point resista	nce.			
I certify that I represent information and that it is	the applicant in the capacity true to the best of my knowled	indicated belonged and belief.	ow and that I h	nave examin	ed the foregoing	statement of technical
Name (Please Print or Ty	pe)		Signature (¢hec	Kappropria	te box below)	
R. Stuart Graham				()		
Address (include ZIP Cod	e)		Date / (X		Andrew Control	
			January 27, 2	2011(
Graham Brock, Inc. P. O. Box 24466		}	Telephone No. (a Code)	
St. Simons Island, GA	A 31522-7466		912-638-802	•	•	
St. Simons Island, Gz	1 31322-7400		712-030-002	·O.		/**************************************
Technical Director		Ε	Registered	Professiona	l Engineer	
Chief Operator		Ē	Technical C	Consultant		
Other (specify)						

FCC 302-AM (Page 5) August 1995

Table of Contents

Exhibit	<u>Description</u>
	Technical Statement
1)	Analysis of Tower Impedance Measurements to Verify Method of Moments Model
2)	Derivation of Operating Parameters for Directional Antenna
3)	Method of Moments Model Details for Towers Driven Individually
4)	Method of Moments Model Details for Directional Antenna
5)	Direct Measurement of Power
6)	Sampling System and Measurements
7)	Reference Field Strength Measurements
8)	Antenna Monitor Calibration
9)	Post Construction Array Geometry Certification
10)	Polar Graph - KTCK Day Pattern
11)	Polar Graph - KTCK Night Pattern
12)	Affidavit of William Guyner
	Affidavit of Richard Graham

This Technical Statement was prepared on behalf of Susquehanna Radio Corp. ("SRC"), licensee of radio station KCTK, 1310 kHz, Dallas, Texas. SRC holds a valid construction permit (BP-20091116ADS) for increased directional daytime power, but with no changes to their licensed directional nighttime operation. BP-20091116ADS authorizes 25.0 kilowatts daytime and continued operation at 5.0 kilowatts nighttime. This application seeks program test authority and a station license with a computer analyzed directional operation under the provisions of Section 73.151(c). The calculations shown herein are for the daytime power of 25.0 kilowatts and the nighttime power of 5.0 kilowatts.

The towers are identified using the nighttime numbering sequence: Tower #1 (northeast), Tower #2 (center east), Tower #3 (southeast) and Tower #4 (west). The towers and ground system were constructed in accordance with the terms of the KCTK construction permit and specifications that were provided in the application for construction permit.

Information is provided herein to demonstrate the directional antenna parameters for the daytime and nighttime authorized patterns are in accordance with the requirements of Section

73.151(c) of the Commission's rules. The system has been adjusted to produce antenna monitor parameters within +/- 5 percent in ratio and +/- 3 degrees in phase of the modeled values, as required by the rules.

There are three special operating conditions and/or restrictions listed on the KTCK construction permit that must be met.

Condition #1 states:

"The permittee must submit a proof of performance as set forth in either section 73.151(a) or 73.151(c) of the rules before program tests are authorized. A proof of performance based on field strength measurements, per Section 73.151(a), shall include a complete nondirectional proof of performance, in addition to a complete proof on the (day) directional antenna system. The nondirectional and directional field strength measurements must be made under similar environmental conditions. The proof(s) of performance submitted to the Commission must contain all of the data specified in Section 73.186 of the rules. Permittees who elect to submit a moment method proof of performance, as set forth in section 73.151(c), must use series-fed radiators. In addition, the sampling system must be constructed as described in Section 73.1515(c)(2)(1)."

This application supports the application for station license using the Moment proof rules of 73.151(c).

Condition #2 states:

"Permittee shall install a type accepted transmitter, or submit application (FCC Form 301) along with data subscribed in Section 73.1660(b) should non-type accepted transmitter be proposed."

The applicant has installed a Harris 3DX25, S/N JW30002037-001 which is type accepted in compliance with this condition.

Condition #3 states:

"Ground system consists of 120 equally spaced, buried, copper radials about the base of each tower, each 85.3 meters in length except where shortened at property boundary and between towers. Each tower has a 7.3 meter ground screen."

The applicant verifies the ground system is as described and accepts this condition.

Field measurements were conducted along the specified monitor point radials for both daytime and nighttime operation and are detailed in Exhibit #7.

During nighttime operation Tower #1 of the array is not used in the directional pattern. By reference to Exhibit #4, Tower #1 has a reactive drive impedance of -j 373.63 Ohms during nighttime operation. Referencing the feed line inductive reactance of +j 32.6 Ohms or 3.96 uHy inductance (Exhibit #1A) a 41.4 uHy coil shunt inductance to ground equivalent to +j 341.0 Ohms equals a conjugate reactance of +j 373.6 Ohms to the drive impedance reactance at the tower in nighttime mode operation. The shunt reactance for this tower effectively de-tunes the towers from radiating any significant power and is included in the Moment analysis of the array.

We have tried to be as accurate as possible in the preparation of this application. All information contained in this application was extracted from the CDBS database. We assume no liability for omissions or errors in this source. Should there be any questions concerning the information contained herein, we welcome the opportunity to discuss the matter by phone at 912-638-8028 or by email at rsg@grahambrock.com.

EXHIBIT #1

Analysis of Tower Impedance Measurements to Verify Method of Moments Model

Tower base impedance measurements were made at the final J-plugs within the Antenna Tuning Units ("ATU's") using an Array Solutions, POWER AIM 120, Vector Impedance Analyzer in a calibrated measurement system. The other towers were short circuited at the same points where impedance measurements were made ("reference points"), in compliance with Section 73.151(c)(1).

The reference point in each ATU is followed by the feed-line that exits the ATU enclosure and is connected to the tower above the base insulator. Circuit calculations were performed to relate the Method of Moments modeled impedances of the tower feed points to the ATU output measurement (reference) points, as shown on the following pages. The XL shown for each tower, which was calculated for the assumed stray inductance, was less than 10 uH, in compliance with Section 73.151(c)(1)(vii).

The modeled and measured base impedances at the ATU output jacks, with the other towers short circuited at their ATU output jacks agree within +/- 2 ohms and +/- 4 percent for resistance, as required by Section 73.151(c)(2) of the FCC Rules.

EXHIBIT #1A

KTCK

Dallas

TX

1310

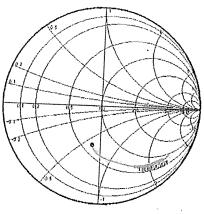
TOWER	L(uH) - series	X(L)	Z(towe	r-mode	led)	Z(ATU	D1000	1)			
1 (ne)	3.96	+i 32.6		1.			-measu	rea)	Z(towe	r-measur	ed)
2 (ce)	5.00		36.4	<u>-j</u>	134,27	36.4	-i	101.71	36.4	i	134.2
		+j 41.2	33.0	-j	146.59	33.0				-	
3 (se)	2.00	+j 16.4	37.3	1			-17	105.41		-j	146.59
4 (w)	4.69	+i 38.6		ار	126.18	37.3	·j	109.73	37.3	l-i	126.18
		1) 30.0	37.6	rj	144.76	37.6	-i	106.13	37.6	i	144.76

From Moment Method Calculated Values

Tower Impedance Tolerance		Resistance & Reactance	+/- 2 Ohms and +/- 4%
Tower	Resistance	(+/- ohms)	High Low
1 (ne)	36.36	3.45	
2 (ce)	32.98	3.32	
3 (se)	37.30	3.49	
4 (w)	37.63	3.51	40.8 33.8 41.1 34.1
	Reactance	(+/- olims)	High Low
1 (ne)	134.27	7.37	141.6 126.9
2 (ce)	146.59	7.86	1
3 (se)	126.18	7.05	154.5 138.7
4 (w)	144.76	7.79	133.2 119.1
		7.79	152.6 137.0

EXHIBIT #1B

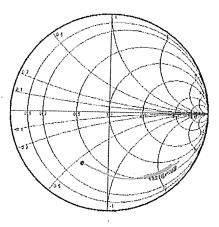
Tower #1 Impedance Measurements



Marker Freq	Rs	Χs
Marker Freq [1] 1.200000 [2] 1.285000 [3] 1.295000 [4] 1.295000 [5] 1.300000 [6] 1.305000 [7] 1.310000 [8] 1.315000 [9] 1.325000 [10] 1.325000 [11] 1.335000	40.953 40.237 39.548 30.024 38.039 37.206 36.361 35.557 34.040 34.278 33.074	Xs -128.594 -124.120 -119.553 -114.975 -110.443 -106.016 -101.713 -97.547 -93.508 -89.571
[13] 1.340000	33.639 33.546	-01.070 -78.025

EXHIBIT #1C

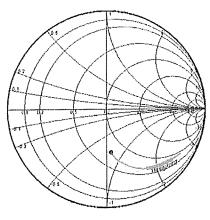
Tower #2 Impedance Measurements



39.731	-127.58
38.713 37.511 36.251 35.039 33.942 32.904 32.146 31.389 30.657 29.900 29.081	-124.366 -121.042 -117.476 -113.666 -109.630 -105.413 -101.079 -96.701 -92.343 -08.063 -03.895 -79.850
	32.146 31.389 30.657 29.900

EXHIBIT #1D

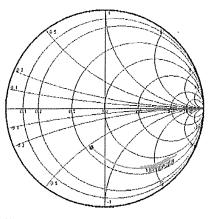
Tower #3 Impedance Measurements



Marker	Freq	Rs	Χs
1 11	1.280000	40.914	-132,986
[2]	1.285000	40,250	-129,493
[3]	1.290000	39,668	-125.873
[4]	1.295000	39,104	-122.077
5]	1.300000	38.534	-118.100
[6]	1,305000	37.934	-113,970
[7]	1.310000	37,296	-109,732
[8]	1.315000	. 36,624	-105.438
[9]	1.320000	35,933	-101.140
[10]	1.325000	35,247	-96.881
[11]	1.330000	34,594	-92,592
[12]	1,335000	34.006	-88.591
[13]	1.340000	33.509	-84,578

EXHIBIT #1E

Tower #4 Impedance Measurements



Marker	Freq	Rs	Xs
[1]	1.200000	42.855	-130.661
[5]	1.285000	42.161	-126,776
[3]	1.290000	41.324	-122.841
[4]	1.295000	40,402	-118,818
[5]	1.300000	39.452	-114,690
[6]	1.305000	38.518	-110.456
[7]	1.310000	37.627	-106,131
8	1.315000	36.793	-101.741
[9]	1.320000	36.013	-97.314
[10]	1.325000	35.282	-92.884
[11]	1.330000	34,589	-88.478
[12]	1.335000	33.925	-84.119
[13]	1.340000	33.289	-79.815

EXHIBIT #2

Derivation of Operating Parameters for Directional Antenna

The Method of Moments model of the array, following verification with the measured individual short circuited base impedances, was utilized for directional antenna calculations. Calculations were made to determine the complex voltage values for sources located at ground level under each tower of the array to produce current moment sums for the towers that, when normalized, equated to the theoretical field parameters of the authorized directional antenna pattern. With these voltage sources, the tower currents were calculated. Twenty-four segments were used for each tower, so that the modeled current pulse at the base of the tower would correspond to the toroid pick-up at the output of the ATU. As the tower structures, sampling pickups, and sampling lines are identical, the antenna monitor ratios and phases corresponding to the theoretical parameters were calculated directly from the modeled tower currents.

EXHIBIT #2A

Daytime Directional Operating Parameters

DAYTIME - REFERENCE TOWER #1

Current Magnitude		Current Phase		Moment Method Calculations of Antenna Monitor Values		r As Adjusted or Values
Tower	(amperes)	(degrees	Ratio	Phase	Ratio	Phase
l (ne)	17.08	-73.06	1.000	0.0	1.000	0.0
2 (ce)	16.54	0.00	0.968	73.1	0.965	72.3
3 (se)	15.02	-134.23	0.879	-61.2	0.883	-61.2
4 (w)	12.58	-176.94	0.737	-103.9	0.735	-103.0

Daytime Operating Parameter Tolerances

	Ratio (5%)		Phase (3°)	
Tower	(+)	(-)	(+)	(-)
l (ne)	1.000	1.000	0.00	0.00
2 (cc)	1.017	0.920	76.06	70.06
3 (se)	0.923	0.835	-58.17	-64.17
4 (w)	0.773	0.700	-100.88	-106.88

Nighttime Directonal Operating Parameters

NIGHTTIME - REFERENCE TOWER #3

	Current	Current	urrent Moment Method Calculations		Antenna Monito	Antenna Monitor As Adjusted Antenna Monitor Values	
	Magnitude	Phase	of Antenna Monito	nna Monitor Values Antenna Monitor			
Tower	(amperes)	(degrees	Ratio	Phase	Ratio	Phase	
1 (ne)	0.15	-101.27	0.021	12.7			
2 (ce)	5.47	0.00	0.770	114.0	0.789	112.5	
3 (se)	7.1	-113.98	1.000	0.0	1.000	0.0	
4 (w)	4.13	-176.89	0.582	-62.9	0.589	-63.0	

Nighttime Operating Parameter Tolerances

	Ratio (5%)		Phase (3°)	
Tower	(+)	(-)	(+)	(-)
l (ne)	**			
2 (ce)	0.809	0.732	116.98	110.98
3 (se)	1.000	1.000	0.00	0.00
4 (w)	0.611	0.553	-59.91	-65.91

EXHIBIT #3

Method of Moments Model Details for Towers Driven Individually

The array of towers was modeled using Westberg Engineering PhasorPro 2.1.1.12. One wire was used to represent each tower. The electrical length of each tower was specified using degrees at the operating frequency of 1310 kHz (1.31 MHz), as taken from the theoretical directional antenna specifications. Each tower was modeled using twenty-four segments. As the towers are 225.4 degrees in electrical height, the segment length is 9.8 electrical degrees, in compliance with Section 73.151(c)(1)(iii).

The individual tower characteristics were adjusted to provide a match of their modeled impedances, when presented to a circuit model, that included branches representing the stray feed-line hookup inductances at the tower bases, with the base impedances that were measured at the output jacks of the ATU's, while the other towers of the array were short circuited. The Method of Moments model assumed loads at ground level having the reactance that was calculated for them using the base circuit models for the open circuited towers of the array.

Each tower's modeled height, relative to its physical height, falls within the required range of 75% to 125%, in compliance with Section 73.151(c)(1)(v). Each tower's modeled

radius falls within the range of 80% to 150% of the radius of a circle having a circumference equal to the sum of the widths of the tower sides, which is in compliance with Section 73.151(c)(1)(i). The array consists of identical, uniform cross section towers having a face of 36 inches.

EXHIBIT #3A

KTCK

Dallas

TX

1310

Γ		Physical	Velocity	Modeled	Modeled	Physical	Modeled	Percent of
ı	Tower	Height	Factor	Height	Percent of	Equivalent	Radius	Equivalent
L		(degrees)	Adjustment	(degrees)	Height	Radius (inches)	(inches)	Radius
Γ	l (nc)	225,4	0.96295	234.07	103.8%	16.628	16.628	100.0%
Г	2 (ce)	225.4	0.97758	230.57	102.3%	16,628	16.628	100.0%
Γ	3 (se)	225.4	0.95465	236.11	104.8%	16.628	16.628	100.0%
Г	4 (w)	225.4	0.97435	231.33	102.6%	16.628	16.628	100.0%

	Tower Height	l'olerance		Tower Radius	Tolerance	
	>75% <125%			>80% <150%		
Tower	Height	Minimum	Maximum	Actual	Minimum	Maximum
1 (ne)	225.4	169.1	281.8	16.628	13.302	24.942
2 (ce)	225.4	169.1	281.8	16.628	13.302	24.942
3 (se)	225.4	169.1	281.8	16.628	13.302	24.942
4 (w)	225.4	169.1	281.8	16.628	13.302	24.942

EXHIBIT #4

Method of Moments Model Details for Directional Antenna Pattern(s)

The array of towers was modeled using Westberg Engineering PhasorPro 2.1.1.12 with the individual tower characteristics that were verified by the individual tower impedance measurements. Calculations were made to determine the complex voltage values for sources located at ground level under each tower of the array to produce current moment sums for the tower that, when normalized, equated to the theoretical field parameters of the authorized directional antenna pattern. The following pages contain details of the method of moments model of the directional antenna patterns.

EXHIBIT #4A

STATION INFORMATION					
Call Letters No. Towers Frequency					
ктск	4	1.3100			

TOWER INFORMATION							
	Tower Height (°)	Spacing (°)	Orientation	Face Width (in.)	Radius (in.)	Velocity Factor	
Tower 1	225.4000	90.0000	0.0000	36.0000 / 36.0000	16.6277 / 16.6277	0.962950	
Tower 2	225.4000	0.0000	0.0000	36.0000 / 36.0000	16.6277 / 16.6277	0.977580	
Tower 3	225.4000	90.0000	180.0000	36.0000 / 36.0000	16.6277 / 16.6277	0.954650	
Tower 4	225.4000	90.0000	290.0000	36.0000 / 36.0000	16.6277 / 16.6277	0.974350	

MATRIX INFORMATION						
	Impedance (other towers open)	Impedance (other towers shorted)				
Tower 1	40.38 - j129.27	36.36 - j134.27				
Tower 2	38.12 - j134.41	32.98 - j146.59				
Tower 3	41.56 - j123.59	37.30 - j126.18				
Tower 4	43.02 - j138.66	37.63 - j144.76				

DETUNED TOWER CURRENTS

Tower 1

0.000000 > 0.000000 - 225.40° above ground 1.084705 > 70.503670 - 215.60° above ground 1.850476 > 70.539553 - 205.80° above ground 2.480974 > 70.597736 - 196.00° above ground 2.969477 > 70.695262 - 186.20° above ground 3.310204 > 70.849939 - 176.40° above ground 3.497084 > 71.082885 - 166.60° above ground 3.526902 > 71.422022 - 156.80° above ground 3.400378 > 71.908992 - 147.00° above ground 3.122664 > 72.614138 - 137.20° above ground 2.703540 > 73.673737 - 127.40° above ground 2.157504 > 75.402209 - 117.60° above ground 1.504439 > 78.746444 - 107.80° above ground 0.776334 > 88.487268 - 98.00° above ground 0,263259 > 177,693502 - 88,20° above ground 0.965433 > -124.258332 - 78.40° above ground 1.814568 > -116.391863 - 68.60° above ground 2.658561 > -112.984049 - 58.80° above ground 3,463759 > -110.694288 - 49.00° above ground 4.204506 > -108.745210 - 39.20° above ground 4.859974 > -106.831772 - 29.40° above ground 5.416100 > -104.763681 - 19.60° above ground 5.865360 > -102.406237 - 9.80° above ground 6.337162 > -98.356584 - -0.00° above ground

Tower 2

0.000000 > 0.000000 - 225.40° above ground 1.058660 > 71.224016 - 215.60° above ground 1.799386 > 71.284017 - 205.80° above ground 2.405394 > 71.367314 - 196.00° above ground 2.871423 > 71.489183 - 186.20° above ground 3.193232 > 71.665107 - 176.40° above ground 3.366141 > 71.913791 - 166.60° above ground 3,388072 > 72,260549 - 156.80° above ground 3.260544 > 72.743858 - 147.00° above ground 2.989120 > 73.429500 - 137.20° above ground 2.583562 > 74.445787 - 127.40° above ground 2.057888 > 76.090106 - 117.60° above ground 1.430905 > 79.262769 - 107.80° above ground 0.731998 > 88.570952 - 98.00° above ground 0.239262 > -178.914950 - 88.20° above ground 0.924236 > -122.302343 - 78.40° above ground 1.737729 > -114.961834 - 68.60° above ground 2.545977 > -111.788765 - 58.80° above ground 3.318357 > -109.665648 - 49.00° above ground 4.031144 > -107.868431 - 39.20° above ground 4.665001 > -106.114277 - 29.40° above ground 5.206952 > -104.228611 - 19.60° above ground 5.649754 > -102.091199 - 9.80° above ground 6.125098 > -98.429836 - -0.00° above ground

DETUNED TOWER CURRENTS

Tower 3

0,000000 > 0.000000 - 225.40° above ground 0.846300 > -6.699737 - 215.60° above ground 1,429461 > -6,262700 - 205.80° above ground 1.896519 > -5.831926 - 196.00° above ground 2,244606 > -5.381083 - 186.20° above ground 2.471889 > -4.892869 - 176.40° above ground 2.576591 > -4.345929 - 166.60° above ground 2.559340 > -3.710168 - 156.80° above ground 2,423896 > -2,937721 - 147.00° above ground 2.177421 > -1.942752 - 137.20° above ground 1.830522 > -0.547844 - 127.40° above ground 1,397310 > 1.693448 - 117.60° above ground 0,896342 > 6.337695 - 107.80° above ground 0.364220 > 24.621998 - 98.00° above ground 0.327789 > 143.272645 - 88.20° above ground 0.899145 > 165.293344 - 78.40° above ground 1.488844 > 170.518756 - 68.60° above ground 2.052778 > 173.170541 - 58.80° above ground 2,568520 > 175.033045 - 49.00° above ground 3.017527 > 176.617571 - 39.20° above ground 3,384270 > 178.150912 - 29.40° above ground 3,656614 > 179,791210 - 19,60° above ground 3.826511 > -178.325091 - 9.80° above ground 3.896443 > -174.946520 - -0.00° above ground

Tower 4

0.000000 > 0.000000 - 225.40° above ground 1,009487 > 59.577456 - 215.60° above ground 1.713473 > 59.671698 - 205.80° above ground 2,286950 > 59,784945 - 196,00° above ground 2.725185 > 59.932087 - 186.20° above ground 3.024463 > 60.127614 - 176.40° above ground 3,180731 > 60.389409 - 166.60° above ground 3.192493 > 60.742018 - 156.80° above ground 3.061755 > 61.223099 - 147.00° above ground 2.794444 > 61.897557 - 137.20° above ground 2,400534 > 62.893374 - 127.40° above ground 1.894085 > 64.512428 - 117.60° above ground 1,293714 > 67,698164 - 107.80° above ground 0.628576 > 77.673396 - 98.00° above ground 0,241966 > -174,963030 - 88,20° above ground 0.927381 > -131.916339 - 78.40° above ground 1.689878 > -125.679274 - 68.60° above ground 2.439458 > -122.860058 - 58.80° above ground 3.148063 > -120.938065 - 49.00° above ground 3,793014 > -119,297197 - 39,20° above ground 4,355532 > -117.688515 - 29.40° above ground 4.822294 > -115.952088 - 19.60° above ground 5.185249 > -113.969924 - 9.80° above ground 5.534503 > -110.523539 - -0.00° above ground

ZMatrix						
40.38 - j129.27	25.74 + j0.29	5.43 - j10.00	23.11 - j3.26			
	38.12 - j134.41	28.01 - j1.56	26.12 + j3.53			
5.43 - j10.00	28.01 - j1.56	41.56 - j123.59	14.29 - j9.50			
23.11 - j3.26	26.12 + j3.53	14.29 - j9.50	43.02 - j138.66			

d e

	YMatrix					
0.001879 + j0.006939	0.000866 - j0.000660	-0.000396 - j0.000721	0.000718 - j0.000789			
0.000866 - j0.000660	0.001461 + j0.006493	0.000968 - j0.000776	0.000816 - j0.000539			
-0.000396 - j0.000721						
0.000718 - j0.000789						

HMatrix - [I] = [H] X [F]					
	-	***	0.00074 . :0.002447		
-0.018081 + j0.007493	0.002902 + j0.004508	0.002783 - J0.000863	0.003271 + 10.003447		
0.002549 + j0.004251	-0.017615 + j0.007997	0.002623 + j0.004130	0.002539 + j0.004485		
0.003008 - j0.000946					
0.003057 + j0.003274	0.002732 + j0.004529	0.003452 + j0.000735	-0.017219 + j0.007714		

HMatrix-inverse - [F] = [H] ⁻¹ X [I]					
-41.528423 - j18.570143	7.209836 - j11.692677	-1.018614 - j3.082646	4.501654 - j10.421446		
	-36.899638 - j16.674223	5.923280 - j11.939023	9.181103 - j11.057273		
-1.226529 - j3.405282		-42.714397 - j19.386304	-0.499967 - j7.800466		
4.359620 - j9.808113	9.043054 - j11.530092	-0.175258 - j6.863687	-41.507716 - j20.512601		

Mode 1

Tower 1

 $0.000000 > 0.000000 - 225.40^{\circ}$ above ground 3.731782 > 112.359630 - 215.60° above ground 6.513849 > 112.768844 - 205.80° above ground 8.949817 > 113.194030 - 196.00° above ground 11.010167 > 113.656662 - 186.20° above ground 12.666488 > 114.170944 - 176.40° above ground 13.886857 > 114.754080 - 166.60° above ground 14.646140 > 115.428707 - 156.80° above ground 14.929697 > 116.226562 - 147.00° above ground 14.735351 > 117.194582 - 137.20° above ground 14.074449 > 118.406101 - 127.40° above ground 12.972462 > 119.983153 - 117.60° above ground 11.469656 > 122.145319 - 107.80° above ground 9.623029 > 125.330283 - 98.00° above ground 7,513617 > 130.541937 - 88.20° above ground 5.277753 > 140.582138 - 78.40° above ground 3.275697 > 165.087350 - 68.60° above ground 2.784356 > -141.217623 - 58.80° above ground 4.480174 > -104.419341 - 49.00° above ground 6.875122 > -90.191905 - 39.20° above ground 9.357574 > -83.320320 - 29.40° above ground 11.768747 > -79.174188 - 19.60° above ground 14.049517 > -76.251487 - 9.80° above ground 17.080741 > -73.064886 - -0.00° above ground

Tower 2 0.000000 > 0.000000 - 225.40° above ground 4.123323 > -172.710522 - 215.60° above ground 7.270913 > -172.493635 - 205.80° above ground 10.098091 > -172.286784 - 196.00° above ground 12.565503 > -172.082736 - 186.20° above ground 14.633958 > -171.878733 - 176.40° above ground 16.258862 > -171.671072 - 166.60° above ground 17.401791 > -171.454511 - 156.80° above ground 18.034802 > -171.221479 - 147.00° above ground 18.142843 > -170.960842 - 137.20° above ground 17.725019 > -170.655697 - 127.40° above ground 16.795077 > -170.279206 - 117.60° above ground 15.381294 > -169.786152 - 107.80° above ground 13.525873 > -169.094204 - 98.00° above ground 11.284131 > -168.036680 - 88.20° above ground 8.724194 > -166.219787 - 78.40° above ground 5.930868 > -162.449355 - 68.60° above ground $3.046060 > -150.853829 - 58.80^{\circ}$ above ground 1.254283 > -69.834308 - 49.00° above ground 3.657209 > -13.984467 - 39.20° above ground 6.652904 > -5.308425 - 29.40° above ground 9.630868 > -2.277838 - 19.60° above ground 12,524982 > -0.884675 - 9.80° above ground

16.539366 > 0.000000 - -0.00° above ground

Mode 1

Tower 3

0.000000 > 0.000000 - 225.40° above ground 3,274269 > 46,325883 - 215.60° above ground 5.724649 > 46.746287 - 205.80° above ground 7.872726 > 47.179822 - 196.00° above ground 9.688831 > 47.648479 - 186.20° above ground 11.144171 > 48.166460 - 176.40° above ground 12.207370 > 48.750674 - 166.60° above ground 12.853725 > 49.423137 - 156.80° above ground 13.068647 > 50.214601 - 147.00° above ground 12,849524 > 51,170673 - 137,20° above ground 12,206690 > 52,363268 - 127,40° above ground 11.163922 > 53.914043 - 117.60° above ground 9.758907 > 56.047614 - 107.80° above ground 8.044776 > 59.229916 - 98.00° above ground 6.096782 > 64.601015 - 88.20° above ground 4.045313 > 75.726975 - 78.40° above ground 2.300009 > 107.327007 - 68.60° above ground 2.408212 > 170.909566 - 58.80° above ground 4,290162 > -159.865817 - 49.00° above ground 6.501744 > -149.194389 - 39.20° above ground 8.685327 > -143.731570 - 29.40° above ground 10.740450 > -140.184808 - 19.60° above ground 12.623545 > -137.474719 - 9.80° above ground 15.016669 > -134.225502 - -0.00° above ground

Tower 4 0.000000 > 0.000000 - 225.40° above ground 2,806235 > -0.495317 - 215.60° above ground 4.879582 > -0.259098 - 205.80° above ground 6.679640 > -0.016449 - 196.00° above ground 8.183786 > 0.245374 - 186.20° above ground 9.370527 > 0.534304 - 176.40° above ground 10.215900 > 0.859523 - 166.60° above ground 10.701507 > 1.232737 - 156.80° above ground 10.817398 > 1.670106 - 147.00° above ground 10.563563 > 2.195523 - 137.20° above ground 9.950581 > 2.846911 - 127.40° above ground 8.999723 > 3.689568 - 117.60° above ground 7.742698 > 4.848063 - 107.80° above ground 6.221370 > 6.596113 - 98.00° above ground 4.488649 > 9.679780 - 88.20° above ground 2.618822 > 17.088266 - 78.40° above ground 0.891262 > 57.816100 - 68.60° above ground 1.747603 > 156.213695 - 58.80° above ground 3.708691 > 170.415633 - 49.00° above ground 5.661393 > 175.044033 - 39.20° above ground 7,504644 > 177,582136 - 29,40° above ground 9,195936 > 179,406933 - 19.60° above ground 10.710287 > -179.039954 - 9.80° above ground

12.584846 > -176.943707 - -0.00° above ground

Mode 2

Tower 1

0.000000 > 0.000000 - 225.40° above ground 0.024409 > -134.160495 - 215.60° above ground 0,036560 > -131.567692 - 205.80° above ground 0.042399 > -128.566375 - 196.00° above ground 0.042783 > -124.864382 - 186.20° above ground 0.038666 > -119.982236 - 176.40° above ground 0,031068 > -112,738563 - 166,60° above ground 0.021316 > -99.382225 - 156.80° above ground 0.012400 > -64.348162 - 147.00° above ground 0,013698 > 1,026423 - 137.20° above ground 0.024260 > 30.980471 - 127.40° above ground 0.035960 > 43,435032 - 117.60° above ground 0.046438 > 50.983815 - 107.80° above ground 0.054604 > 56.749208 - 98.00° above ground 0,059669 > 61.807037 - 88.20° above ground 0.060989 > 66.690006 - 78.40° above ground $0.058042 > 71.831335 - 68.60^{\circ}$ above ground 0.050436 > 77.896140 - 58.80° above ground 0.037988 > 86.694186 - 49.00° above ground 0,021448 > 107.191758 - 39.20° above ground 0.014674 > -166.419931 - 29.40° above ground 0.040387 > -121.130563 - 19.60° above ground 0.077832 > -109.204537 - 9.80° above ground 0.146199 > -101.276854 - -0.00° above ground

Tower 2

0.000000 > 0.000000 - 225.40° above ground 1,359967 > -175,007907 - 215,60° above ground 2,393924 > -174.864319 - 205.80° above ground 3.318909 > -174.729483 - 196.00° above ground 4,122201 > -174.598842 - 186.20° above ground 4.791186 > -174.470864 - 176.40° above ground 5.311539 > -174.343413 - 166.60° above ground 5,671046 > -174,213377 - 156,80° above ground 5,861025 > -174,076170 - 147,00° above ground 5,877108 > -173,924946 - 137,20° above ground 5.719644 > -173.749164 - 127.40° above ground 5,393832 > -173,531826 - 117.60° above ground 4,909647 > -173,243779 - 107.80° above ground 4.281583 > -172.830731 - 98.00° above ground 3.528268 > -172.179382 - 88.20° above ground 2.672062 > -171.009424 - 78.40° above ground 1,739241 > -168,395630 - 68.60° above ground 0.767708 > -158.584697 - 58.80° above ground 0.368713 > -35.175453 - 49.00° above ground 1.327752 > -6.467902 - 39.20° above ground 2.319100 > -2.346552 - 29.40° above ground 3.282712 > -0.894498 - 19.60° above ground 4.206855 > -0.279455 - 9.80° above ground 5.470438 > 0.000000 - -0.00° above ground

Mode 2

Tower 3

0.000000 > 0.000000 - 225.40° above ground 1.590479 > 68.308935 - 215.60° above ground 2.774242 > 68.685172 - 205.80° above ground 3.806912 > 69.074054 - 196.00° above ground 4.675334 > 69.495790 - 186.20° above ground 5.366867 > 69.963773 - 176.40° above ground 5.867629 > 70.494084 - 166.60° above ground 6.166942 > 71.107788 - 156.80° above ground 6.258925 > 71.834453 - 147.00° above ground 6.143344 > 72.718112 - 137.20° above ground 5.826028 > 73.828449 - 127.40° above ground 5,319060 > 75.283740 - 117.60° above ground 4.640945 > 77.303092 - 107.80° above ground 3.817263 > 80.342865 - 98.00° above ground 2.883660 > 85.526513 - 88.20° above ground 1.901015 > 96.411605 - 78.40° above ground 1.062182 > 128.181409 - 68.60° above ground 1.122992 > -166.755022 - 58.80° above ground 2.028226 > -138.003102 - 49.00° above ground 3.080052 > -127.749712 - 39.20° above ground 4,114685 > -122.586452 - 29.40° above ground 5.086394 > -119.300761 - 19.60° above ground 5.975058 > -116.847892 - 9.80° above ground 7.100797 > -113.983961 - -0.00° above ground

Tower 4 0.000000 > 0.000000 - 225.40° above ground 0.927502 > 3.155362 - 215.60° above ground 1.620083 > 3.611360 - 205.80° above ground 2.228064 > 4.071846 - 196.00° above ground 2.743507 > 4.558140 - 186.20° above ground 3.158751 > 5.082237 - 176.40° above ground 3.465215 > 5.658298 - 166.60° above ground 3.656036 > 6.304672 - 156.80° above ground 3.727034 > 7.046830 - 147.00° above ground 3.677235 > 7.922164 - 137.20° above ground 3.509130 > 8.988867 - 127.40° above ground 3,228796 > 10.343789 - 117.60° above ground 2.845951 > 12.162169 - 107.80° above ground 2.374159 > 14.798159 - 98.00° above ground 1.831860 > 19.088470 - 88.20° above ground 1.247593 > 27.538435 - 78.40° above ground 0.695516 > 50.826036 - 68.60° above ground 0.546599 > 117.222136 - 58.80° above ground 1.030659 > 156.097915 - 49.00° above ground 1.652788 > 168.336212 - 39.20° above ground 2.275160 > 174.047566 - 29.40° above ground 2.867035 > 177.556578 - 19.60° above ground 3.416204 > -179.868710 - 9.80° above ground 4.130626 > -176.884900 - -0.00° above ground

FIELD INFORMATION - DAY				
	Field Ratio	Field Phase		
Tower 1	0.6770	-63.0000		
Tower 2	1.0000	0.0000		
Tower 3	0.5530	-131.0000		
Tower 4	0.4120	173.0000		

į.

FIELD INFORMATION - NIGHT			
	Field Ratio	Field Phase	
Tower 2	1.0000	0.0000	
Tower 3	0.8500	-105.0000	
Tower 4	0.5200	188.0000	

TOWER DRIVE INFORMATION - DAY					
	Field Ratios	Field Phase	Drive Imped. (Ω)	Current	Power (W)
Tower 1	0.6770	-63.0000	35.57 - j129.72	17.08 ∡ -73.06	10376.8338
Tower 2	1.0000	0.0000	7.69 - j180.73	16.54 ∡ 0.00	2103.7284
Tower 3	0.5530	-131.0000	37.61 - j114.33	15.02 ∡ -134.23	8481.8062
Tower 4	0.4120	173.0000	25.49 - j106.71	12.58 ∡ -176.94	4037.6317

TOWER DRIVE INFORMATION - NIGHT					
	Field Ratios	Field Phase	Drive Imped. (Ω)	Current	Power (W)
Tower 1	0.0000	0.0000	65.21 - j373.63	0.15 ∡ -101.27	1.3937
Tower 2	1.0000	0.0000	1.82 - j171.21	5.47 ∡ 0.00	54.3168
Tower 3	0.8500	-105.0000	32.91 - j113.48	7.10 ∡ -113.98	1659.3342
Tower 4	0.5200	188.0000	34.28 - j126.25	4.13 ∡ -176.89	584.9553

January 2011

EXHIBIT #5

Direct Measurement of Power

KCTK will operate with a directional daytime power of 25.0 kilowatts and a common point impedance of 49.7 +/-J 1.0 ohms and a nighttime power of 5.0 kilowatts and a common point impedance of 49.5 +/- J 1.7 ohms.

Daytime

Due to the daytime directional antenna operation, the common point input powers are adjusted with reference to the transmitted power, in accordance with Section 73.51(b)(2)¹.

Adjusting the input power by 1.053 results in the following:

25,000 Watts X 1.053 = 26,325 Watts

Common Point Resistance = 49.7 Ohms

Manipulating $I^2R = P$

Where I = Common Point Current R = Common Point Resistance

P = Power in Watts

 $I = (26,325/49.7)^{5} = 23.0$ Amps at Common Point

The daytime directional power will be monitored at the common point.

Section 73.51 Determining operating power. (b) The authorized antenna input power for each station shall be equal to the nominal power for such station, with the following exceptions: (2) For stations with nominal powers in excess of 5 kilowatts, the authorized antenna input power to directional antennas shall exceed the nominal power by 5.3 percent.

Nighttime

The nighttime directional antenna is licensed with an Antenna Input Power of 2.3 kilowatts of power to achieve a nominal power of 5.0 kilowatts in accordance with the outstanding station license (BZ-20031016ACJ).

2,300 Watts

Common Point Resistance = 49.5 Ohms

Manipulating $I^2R = P$

Where I = Common Point Current R = Common Point Resistance

P = Power in Watts

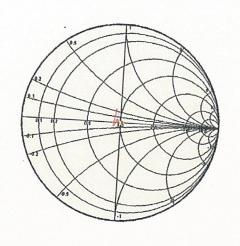
 $I = (2,300/49.5)^{0.5} = 6.82$ Amps at Common Point

The nighttime directional power will be monitored at the common point.

Common point impedance was measured utilizing an Array Solutions, POWER AIM 120, Vector Impedance Analyzer in a calibrated measurement system.

EXHIBIT #5A

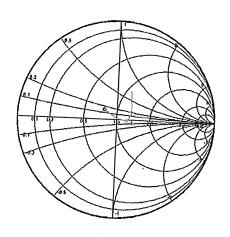
<u>Daytime Common Point Measurements / Impedance</u>



Marker Freq [1] 1.295000	Rs	Xs
[2] 1.300000	45,438	-0,63
[3] 1.305000	47.309	1.51
[4] 1.310000	48,568	0.21
[5] 1.315000	49.701	-0.980
[6] 1.320000	50.151	-0.733
[7] 1.325000	50.620	-0.420
	51.190	0.330

EXHIBIT #5B

Nighttime Common Point Measurements / Impedance



Marker Freq		
[1] 1.295000	Rs	Xs
[2] 1.300000	64.072	3.134
[3] 1.305000	60.710	-1.299
[4] 1.310000	55.130	0.159
[5] 1.315000	49.506	1.715
[6] 1.320000	43.521	5.300
171 1.325000	37.869	8.096
	33.707	11.101

EXHIBIT #6

Sampling System And Measurements

The sample system for KCTK consists of electrical equal lengths of Andrew LDF4-50A phase stabilized coaxial transmission lines terminated into Delta TCT-3 toroid sample transformers. A tabulation of the sample line lengths and characteristic impedances are included in Exhibit #6A.

Impedance measurements of the antenna monitor sampling lines with the toroid sample transformers attached were made using an Array Solutions, POWER AIM 120, Vector Impedance Analyzer in a calibrated measurement system. The impedance at the input to the sample lines, terminated by the toroid sample transformers, was measured and tabulated in Exhibits #6B, #6C, #6D and #6E.

Impedance measurements of the antenna monitor sampling lines were made using an Array Solutions, POWER AIM 120, Vector Impedance Analyzer in a calibrated measurement system. The measurements were made looking into the antenna monitor ends of the sampling lines without the sampling lines connected to the toroid samples under open-circuited conditions. Exhibits #6F, #6G, #6H and #6I detail the sample transmission line measurements with

frequencies above and below carrier frequency where resonance (zero reactance corresponding with low resistance) was found. As the length of a distortionless transmission line is 180 electrical degrees at the difference frequency between adjacent frequencies of resonance and frequencies of resonance occurring at odd multiples of 90 degrees electrical length. The sampling line length calculated from the resonant frequency closest to the carrier frequency was found to be between 336.9 and 337.1 electrical degrees, within the 1.0 degree variance, as specified by Section 73.151(c)(2)(i).

In order to determine the characteristic impedance values of the sampling lines, open-circuit measurements were made with frequencies offset to produce +/- 45 degrees of electrical length from resonance. The characteristic impedance was calculated using the following formula where $R_1 + jX_1$ and $R_2 + jX_2$ are the measured impedances at the +45 and -45 degree offset frequencies, respectively:

$$Z0 = ((R_1^2 + X_1^2)^{1/3} * (R_2^2 + X_2^2)^{1/3})^{1/3}$$

The sampling line characteristic impedance was found to be between 50.7 and 50.9 Ohms, within the 2.0 ohm variance, as specified by Section 73.151(c)(2)(i).

Toroid current transformer calibration was checked by placing each transformer in line at the transmitter output connected to a dummy load. The transformers were connected to the station's antenna monitor with short equal length transmission line jumpers. The relative ratio and phase of all transformers was found to compare identically to each other, within the manufacturer' specifications.

EXHIBIT #6A

KTCK

Dallas

TX

1310

kHz

Sample Line - Andrew Phase Stabilized LDF4-50J

Sample Line and Sample Transformer Combined Impedance at 1310 kHz

Tower Sample System	Sample Transformer Make / Type / Serial #	Resistance (ohms)	Reactance (ohms)	Supporting
1 (ne)	Delta / TCT-3 / 17845	51.01		Exhibit
2 (ce)	Delta / TCT-3 / 17847	51.01	-1.30	6B
3 (se)	Delta / TCT-3 / 17830	50.96 50.89	-1.19	6C
4 (w)	Delta / TCT-3 / 17825	50.93	-1.21	6 1 D
		30,33	-1.29	6E

Sample Line Length and Impedance Calculations

Tower Sample Line	Open Circuit Resonance (kHz)	Calculated Electrical Length at 1410 kHz	Measured Characteristic	Supporting
1 (ne)	1.049608	(degrees)	Impedance	Exhibit
2 (ce)	1.049288	337.0	50.9	6F
3 (se)	1.049927	337.1	50.8	6G
4 (w)	1.049928	336.9	50.7	6Н
			50,8	61

Sample Line Lengths: +/-

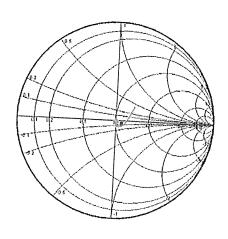
0.10 Degrees : Limit +/- 0.5°

Characteristic Impedance: +/-

0.10 Ohms : Limit +/- 1.0 Ohms

EXHIBIT #6B

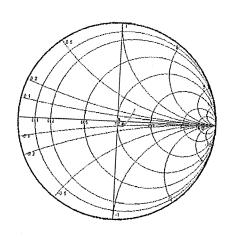
Tower #1 Sample and Toroid



Marker Freq	Rs	Χs
	51.053	-1,303
[2] 1.290000 [3] 1.300000	51.041	-1.307
[4] 1.310000	51.027	-1.306
[5] 1.320000	51.012	-1.300
[6] 1.330000	50.996	-1.289
[7] 1.340000	50.979	-1.274
	50.961	-1.255

EXHIBIT #6C

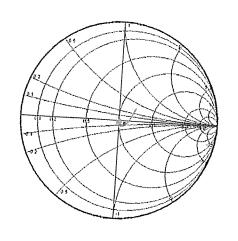
Tower #2 Sample and Toroid



Marker Freq [1] 1.280000	Нв	Xs
[2] 1.290000	50.994	-1.187
[3] 1.300000	50.984	-1.191
[4] 1.310000	50.973	-1.190
5 1.320000	50.962	-1.185
[6] 1.330000	50,949	-1.176
17] 1.340000	50.935	-1.162
	50.921	-1.145

EXHIBIT #6D

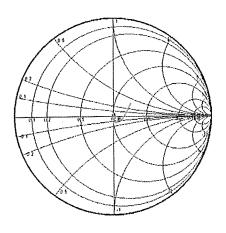
Tower #3 Sample and Toroid



Marker Freq [1] 1.280000	Rs	Χş
[2] 1.290000	50.924	-1.211
1 31 1.300000	50.914	-1.214
4 1.310000	50.903	1.213
1 51 1.320000	50.891	-1.207
[6] 1.330000	50.878	-1.198
7 1.340000	50.864	-1.184
	50.649	-1.167

EXHIBIT #6E

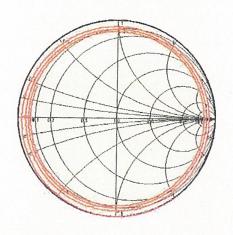
Tower #4 Sample and Toroid



Marker Freq		Нs	Xs
[1] 1.2830	00	50.965	-1.297
[2] 1.2900	00	50.954	-1.300
[3] 1.3000	80	50.941	-1.300
[4] 1.3100	00	50.928	-1.294
[5] 1.3200	00	50.914	-1.285
[6] 1.3330	00	50.899	-1.271
[7] 1.3430	00	50.883	-1.253

EXHIBIT #6F

KCTK Sample Line - Tower #1



Marker	Freq	Rs	Xs
[1]	0.874673	3.217	-50.931
[2]	1.049600	1,968	0.000
1 31	1.224543	5.073	50.402
[4]	1.752982	2.693	-0.000

	Station	Freq	(MHz)
	1.31		

Resonant Freq (MHz)

Resonant Freq (MHz) 1.752982

Closest To Station Freq

1.049608

Line Velocity Factor From Mfg. (%)

1.049608

Length of Line ° @ Station Freq

88

Calculated Physical Length

618.7

feet

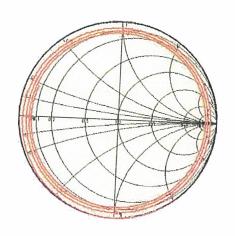
337.0

Impedance at Offset Freq

		1	
-45° Offset (MHz)	Resistance	Reactance	Line Characteristic Impedance (Ohms)
0.874673	3.217	-50.931	(omis)
+45° Offset (MHz)			50.9
1.224543	5.391	50 570	30.9

EXHIBIT #6G

KCTK Sample Line - Tower #2



Marker	Freq	Rs	Χs
	0.674407	3,203	-50.930
	1.049288	2.042	0.000
	1.224169	5.265	50.291
[4]	1.752901	2.728	0.000

Station Freq (MHz)

1.31

Resonant Freq (MHz)

1.049288

Resonant Freq (MHz)

1.752901

Closest To Station Freq

1.049288

Length of Line ° @ Station Freq

337.1

Line Velocity Factor From Mfg. (%)

Calculated Physical Length

618.9

feet

-45° Offset (MHz)

0.874407

Resistance 3.203

Impedance at Offset Freq Reactance

+45° Offset (MHz)

-50.930

Line Characteristic Impedance (Ohms)

1.224169

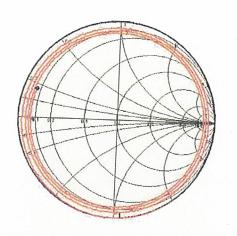
5.265

50.291

50.8

EXHIBIT #6H

KCTK Sample Line - Tower #3



Marker	Freq	Rs	
[11	0.874939	112	Xs
	1.049927	3.158	-50.735
	1.224915	2.074	0.000
	1.753824	5.013	50.395
1 -1	11733024	2.711	-0.000

Station Freq (MHz)

1.31

Resonant Freq (MHz)

1.049927

Resonant Freq (MHz)

1.753824

Closest To Station Freq

1.049927

Length of Line ° @ Station Freq

336.9

Line Velocity Factor From Mfg. (%)

88

Calculated Physical Length

618.6

feet

-45° Offset (MHz)		Impedance at Offset Freq
- stoot (MITE)	Resistance	Resotance

0.874939 +45° Offset (MHz)

1.224915

3.158

-50.735

Line Characteristic Impedance (Ohms)

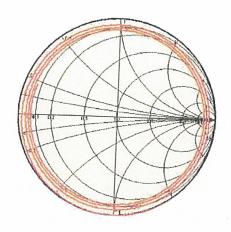
5.013

50.395

50.7

EXHIBIT #61

KCTK Sample Line - Tower #4



Marker	Freq		
		Rs	Χs
-	0.874940	3,111	-50.826
[5]	1.049928	1.965	
[3]	1.224916		0.000
1 41	1.753796	5.029	50.349
		2.690	0.000

Station Freq (MHz)

1.31

Resonant Freq (MHz)

1.049928

Resonant Freq (MHz)

1.753796

Closest To Station Freq

1.049928

Length of Line ° @ Station Freq

336.9

Line Velocity Factor From Mfg. (%)

88

Calculated Physical Length

618.6

feet

-45° Offset (MHz)

0.874940

Resistance 3.111

Impedance at Offset Freq Reactance

Line Characteristic Impedance (Ohms)

+45° Offset (MHz)

-50.826

50.8

1.224916

5.029

50.349

EXHIBIT #7

Reference Field Strength Measurements

Reference field strength measurements were made at three locations along radials on the station monitor point azimuths as specified in the construction permit for the daytime array. In addition three locations were measured in the station's daytime major lobe of 256.5°. Reference field strength measurements were made at three locations along radials on the station monitor point radials as specified in the station license for the nighttime array. In addition three locations were measured in the station's nighttime major lobe of 247.5°. The tabulated measured field strengths, descriptions and GPS coordinates for the reference measurement points during nighttime operation are attached as Exhibit 7A. The GPS unit used was a Delorme LT-40 with Delorme Street Atlas 2008 system with WAAS activated, Datum NAD '83, CONUS and coordinate format DD-MM-SS.s.

Monitor Point Radial Specified on Construction Permit		2000	Cilli)	Dist (km)	m//m	Time (24 hr)	Date	Description
1	ified on Construction 32-57-39.1	n Permit 96-54-26.8	2.17	3.49	135.00	1056	1/24/2011	Driveway of 1613 Dentan De
59.0 2	32-58-17.4	96-53-10.2	3.63	5.84	120.00	1023	1/24/2011	Wet Bound Kallar Coning Marie 611
59.0	32-58-41.6	96-52-23.3	4.52	7.28	80.00	1014	1/24/2011	on Bridge over Hutton Branch Sidewalk - 2239 Souther Circle - 20 ft from Kelly Blvd.
Monitor Point Radial Specified on Construction Permit 179.5 1 32-54-11.4 96-56-	fied on Construction 32-54-11.4	Permit 96-56-18.5	2.86	4.61	105.00	1520	1/24/2011	Sidewalk - 430 I.a Villera Rh.d
179.5	32-53-09.5	96-56-22.0	3,40	5.47	80.00	1500	1/24/2011	Sidewalk - Building 3 Strite 112
179.5	30-39-42.2	88-03-43.0	3.12	5.02	31.00	1320	1/24/2011	Dallas Communications Complex North side Customer Way by Fire Plug beside Nieman Marcus Direct Mail Center
Monitor Point Radial Specified on Construction Permit 350.0 1 32-57-57.3 96-56	ied on Construction 32-57-57.3	Permit 96-56-43.4	1.51	2,44	350.00	1135	1747011	2 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
350.0 2	32-59-37.9	96-57-02.1	3.48	5.60	80.00	1107	1/24/2011	Driveway Hank Haney Colf Bonch
350.0 3	33-00-33.2	96-57-34.8	4.63	7.44	27.00	1528	1/26/2011	Intersection of drive to adjacent property Parking Lot DCT Hebron Station
Geographic Coordinates Datum: NAD '83 CONUS Latitude and Longitude Format: DD-MM-SS s	m: NAD '83 CONU at: DD-MM-SS s	Sí	Ŋ	PS: Delorme LT	40 with Delorm	GPS: Delorme LT-40 with Delorme Street Atlas 2008 ; WAAS Enabled	8 : WAAS En	pajqe
FIM: Potomac : FIM-41 : SN 571 : Calibrated 07/02/97	571 : Calibrated 07/	/02/97	斑	Field Measurements: Bill Guyger	s: Bill Guyger			

Daytime Array Field Measurements

Ķ

Dallas

KTCK 1310 APPLICATION FOR STATION LICENSE
SUSQUEHANNA RADIO CORP.
KTCK AM RADIO STATION
1310 kHz - 5.025.0 kW DA2
BP-20091116ADS
DALLAS, TEXAS
January 2011

APPLICATION FOR STATION LICENSE SUSQUEHANNA RADIO CORP. KTCK AM RADIO STATION 1310 kHz - 5.0/25.0 kW DA2 BP-20091116ADS DALLAS, TEXAS

	1405 Balting @ Court 1 0.	Entry Drive near small creek	Can will be the sound of the N. Royal Lane	North Shoulder of West Bound North Airfield Drive	nabled	
	1/24/2011	1/24/2011		1/24/2011	2008 : WAAS E	
	1155	1304	1311	1101	me Street Atlas	
	238.00	192,00	175.00		GPS: Delorme LT-40 with Delorme Street Atlas 2008 : WAAS Enabled	Field Measurements: Bill Gnyger
	5.20	7.69	8.89		GPS: Delorme I	Field Measurem
	3.23	4.78	5.52			
	96-59-38.4	97-01-11.4	97-01-56.2		NS	7/02/97
	32-56-01.1	32-55-41.9	32-55-32,8		Geographic Coordinates Datum: NAD '83 CONUS Latitude and Longitude Format: DD-MM-SS.s	FIM: Potomac: FIM-41: SN 571: Calibrated 07/02/97
Major lobe Radial - Daytime	1	7	т		oordinates Datun ongitude Format	: FIM-41 : SN 5
Major lobe Ra	256.5	256.5	256.5		Geographic Co Latitude and L	FIM: Potomac

Field Measurements: Bill Guyger

EXHIBIT #7C APPLICATION FOR STATION	08 : WAAS En	GPS: Delorme LT-40 with Delorme Street Atlas 2008; WAAS Enabled Field Measurements; Bill Guyger	40 with Delorm Is: Bill Guyger	GPS: Delorme LT-40 with Delon Field Measurements: Bill Guyger	ÖE	2/97	Latitude and Longitude Format: DD-MM-SS.s. FIM: Potomac: FIM-41: SN 571: Calibrated 07/02/97	ude Format: 141 : SN 57
3697 Stockton Dr	1/26/2011	1540 15 Street Atlac 200	22.20 40 with Delorm	o.ou PS: Delorme I.T.			5	tates Datum;
		,	, ,	000	4 97	96-56-56.5	33-00-58.3	e
Sandy Lake Road to left off main entry. SE Comer of Parking lot of 3301 1-35East.	1/26/2011	1115	13.20	5.27	3.27	96-56-48.0	32-59-28.9	7
Driveway Elm Fork Nature Preserve leading to Picnic Area / Soccor Field. South Side of	1/26/2011	1128	22.80	2.33	1.45	96-56-30.9	32-57-54.7	<u> </u>
						na .	Monitor Point Radial Specified on Station License	ial Specified
Berm on Gateway Drive, 75 ft East of Beltline fron of 6220 Beltline Suite 110.	1/26/2011	1791	00.00	Ŝ.	<u>}</u>			
	1,000,001	1627	110 00	7.36	4.58	96-59-26.0	32-53-37.5	'n
parking lot for PetSmart & Office Depot. South End of Bridge on North Bound Royal Ln.	1/26/2011	1635	150.00	6.02	3.74	96-58-52.3	32-54-10.8	71
NE Comer of Market Place Blvd & Walton Blvd.	1/26/2011	1650	221.00	3.71	2.31	96-57-54.8	32-55-08.3	
corner of Citi Financial Parking Lot						9	Monitor Point Radial Specified on Station License	lial Specified
NE Comer of Royal Ln. & Las Colinas Blvd	1/26/2011	1720	76.00	5.42	3.37	96-57-03.7	32-53-47.7	т
Parking Lot Top of Storm Drain East Bound La Villita Rd.	1/26/2011	1710	118.00	4.53	2.82	96-56-55.4	32-54-15.9	71
SW Corner of Ranch View High School	1/26/2011	1700	150.00	3.09	1.92	96-56-45.6	32-55-2.1	
						Sc	Monitor Point Radial Specified on Station License	dial Specifie
Drive of Akzonobel Paint Plant 2204 Kelly Blvd. on Water Meter	1/26/2011	1500	5.00	6.55	4.07	96-52-39.3	32-58-18.3	m
off Denton Drive, S. Side of Cotton East Side of Josey Ln at Private Enfrance	1/26/2011	1507	10.00	5.19	3,23	96-53-23.3	32-57-58.4	7
Cotton Street at Entrance of 1st Driveway	1/26/2011	1518	12.00	3.46	2.15	ıse 96-54-24.9	recursor of Station License 62.5 1 32-57-31.9 9	idiai Specifie
Description	Date	Time (24 hr)	mv/m	Dist (km)	Dist (mi)	W. Longitude	N. Latitude	Point #
				į			N I stitude	

Nighttime Array Field Measurements

Ķ

Dallas

KTCK 1310

APPLICATION FOR STATION LICENSE SUSQUEHANNA RADIO CORP. KTCK AM RADIO STATION 1310 kHz - 5.025.0 kW DA2 BP-20091116ADS DALLAS, TEXAS January 2011

North shoulder of North Airfield Drive adjacent to FedEX facility.	1/26/2011 2008 : WAAS En	1255 ne Street Atias 2	GPS: Delorme LT-40 with Delorme Street Atlas 2008 : WAAS Enabled	GPS: Delorme [sn	Geographic Coordinates Datum: NAD '83 CONUS Latitude and Longitude Format: DD-MM-SS.5	rdinates Datun ngitude Forma	Geographic Coordinates Datt Latitude and Longitude Form
parking lot at 8300 Esters North shoulder of North Airfield Drive adjacent	1/26/2011	1255	107.00	8.03	4.99	97-01-09.4	52-55-01.0 97-01.	n) : :
Beltline Road, 50 ft North Of Hackberry NE Corner of Royal Ln. & Esters Rd.	1/26/2011	1242	85.00	6.86	4.26	97-00-27.5	32-55-15.3	, 2	247.5
Abandoned Drive - Hackberry Drive, East of	1/26/2011	7071	٠			2 20 00 20		7	247.5
,	1,000,701	1202	122.00	5.40	3.35	96-59-34.9	32-55-33,5		247.5

Major lobe Radial - Nighttime

Field Measurements: Bill Guyger

FIM: Potomac : FIM-41 : SN 571 : Calibrated 07/02/97

EXHIBIT #8

Antenna Monitor Calibration

The antenna monitor at the site is a Potomac Instruments AM-1901, SN 109 and was calibrated on site according to the manufacturer's specifications.

EXHIBIT #9

Summary of Post-Construction Certified Array Geometry

The tower relative distances, provided in feet on the Certified Survey, are converted to electrical degrees at 1310 kHz and used, along with the survey tower azimuths relative to True North, to calculate the distances in electrical degrees from the location specified in the theoretical directional antenna pattern array geometry. Below is a tabulation showing those distances and other data that is relevant to their determination.

75		pecified Array Geome	try	Post-Construction Ce	diffestion*	C C 27 - 4.75	
Tower	Spacing (degrees)	Spacing (feet)	Azimuth (degrees true)	Spacing (feet)	Azimuth (degrees true)	From Specified Base	
l (ne)	90.00	187.83	0.00			(feet)	(degrees)
2 (ce)	0.00	0.00	0.00	189.26 0.00	359.77	1.43	0.23
3 (se)	90.00	187.83	180,00	189,54	0.00	0.00	0.00
4 (w)	90.00	187.83	290.00	189.35	179.57	1.71	0.43
					289.77	1.52	0.23

Tolerance - Distance from Specified Base - 1.5° Survey Variance in Feet / Degrees @ 1310 kHz

Tower	Feet	* @ 1310 kHz
1	1.62	0.78
2	0.00	0.00
3	2.21	1.06
4	1.69	0.81

The "as built" tower displacements from their specified locations expressed in electrical degrees at carrier frequency, which corresponds to space phasing differences in the far-field radiation pattern of the array, are well below the +/- 3 degree operating phase range specified for antenna monitor parameters by the FCC Rules.



January 25, 2011 AVO 27523 SG01

Cumulus Media Partners 900 E. Ledbetter Drive Coppell, TX 75019

Attn: Mr. Bill Guyger

Re: Geodetic location of four radio towers for KTCK radio station located at 900 E. Ledbetter Drive in Coppell, Texas.

Bill:

As requested, please find below the results of our calculations showing the geodetic location of and positioning, by azimuth from north and distance of towers 1, 3, and 4 from tower 2 for the four radio towers located at the referenced site.

Tower No.	Latitude	Longitude	Ground Elevation
1	32 56 41.83 N	96 56 23.46 W	434 ft
2	32 56 39.96 N	96 56 23.46 W	434 ft
3	32 56 38.08 N	96 56 23.46 W	435 ft
4	32 56 40.60 N	96 56 25.55 W	434 ft

From the reference Tower #2

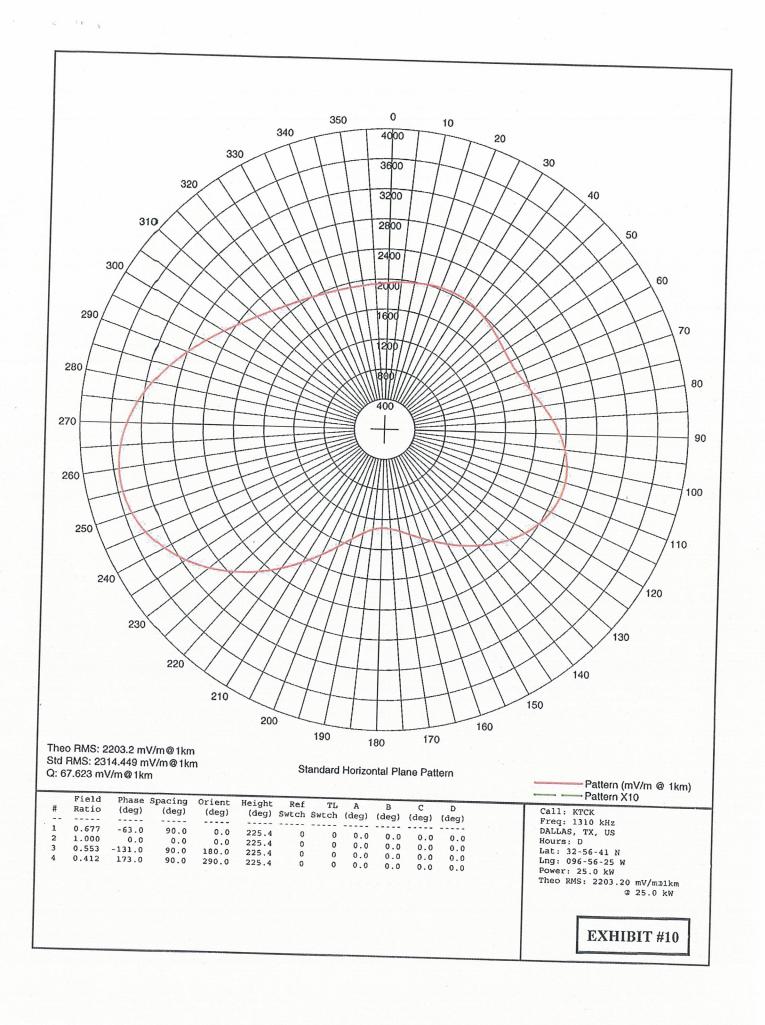
To Tower 1: 189.26 feet on a bearing (Azimuth) from True North of 359.7654 degrees 189.54 feet on a bearing (Azimuth) from True North of 179.5733 degrees 189.35 feet on a bearing (Azimuth) from True North of 289.7739 degrees

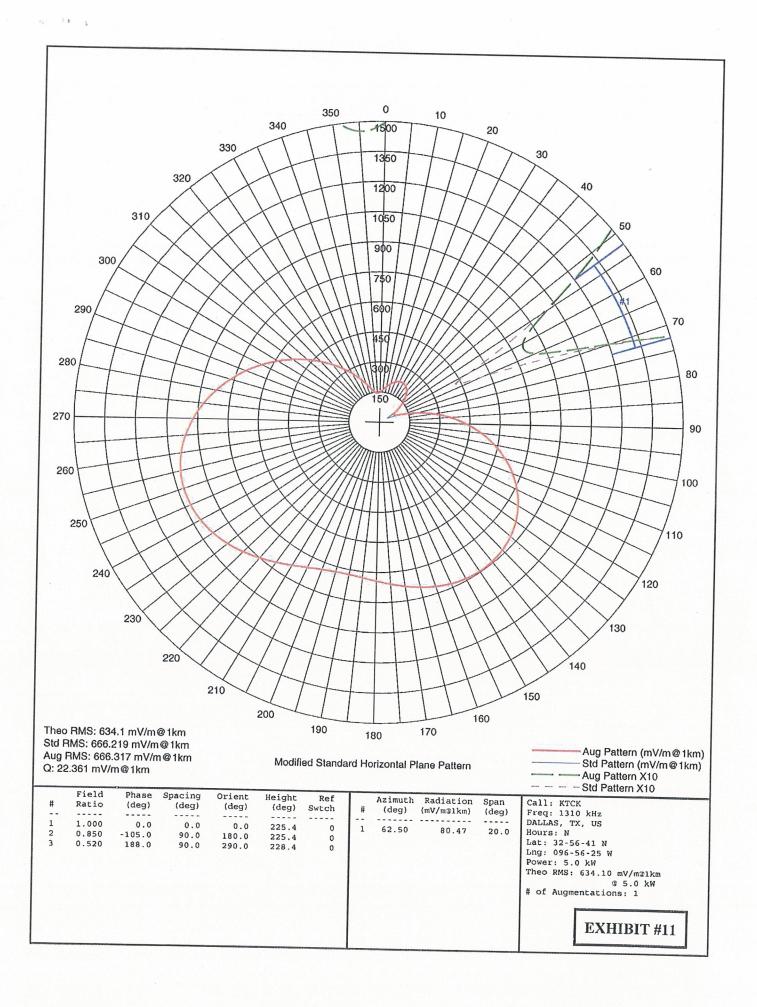
The geodetic values are North American Datum of 1927 (NAD27) using GPS surveying technology. GPS data was obtained using Real Time Kinematic (RTK) surveying from a Virtual Reference Station (VRS) network maintained by Western Data Systems. Three Texas Department of Transportation GPS satellite stations were located and tied into for a horizontal check. Elevations are GPS derived and are relative to the North American Vertical Datum of 1988 (NAVD88).

Sincerely,

HALFF ASSOCIATES, INC.

Andrew J. Shafer, RPLS Survey Department Manager





The State of Texas The County of Dallas

William M. Guyger Jr., having been duly sworn, states the following:

That he is employed by Cumulus Media Partners, Inc. to conduct Antenna System, Sample System, and Field Measurements on Radio Station KTCK. 1310 kHz.

That he is familiar with the operation of the test equipment used as well as the proper Methods and procedures used to conduct antenna system measurements, sample system measurements, and field strength measurements on AM Radio Stations.

That he personally conducted field intensity measurements between January 24 and January 26 of 2011, on Radio Station KTCK; and that he personally conducted measurements on the Antenna and Sampling System and Transmission System of Radio Station KTCK between December 9 and December 29 of 2010.

That the equipment used in conducting these measurements used in conducting these measurements was as follows:

Potomac Instruments FIM-41 S/N 365 last calibrated 07/02/97 Delta Electronics OIB-3 S/N 571 last calibrated 09/24/98 Array Solutions PA120 S/N 1145

That all data relating to these measurements is true and correct to the best of his knowledge;

This the 26th day of January, 2011

Signature

Sworn to and subscribed before me This 2k day of Jan 2011

Anna Berger Votary Public, State of Texas My Commission Expires:

> EXHIBIT #12 APPLICATION FOR STATION LICENSE SUSQUEHANNA RADIO CORP. KTCK AM RADIO STATION 1310 kHz - 5.0/25.0 kW DA2 BP-20091116ADS DALLAS, TEXAS January 2011

AFFIDAVIT AND QUALIFICATIONS OF CONSULTANT

State of Georgia)
St. Simons Island) ss
County of Glynn)

a tribe

R. Stuart Graham, being duly sworn, deposes and says that he is an officer of Graham Brock, Inc. Graham Brock has been engaged by Susquehanna Radio Corp., to prepare the attached Technical Exhibit.

His qualifications are a matter of record before the Federal Communications Commission. He has been active in Broadcast Engineering since 1979.

The attached report was either prepared by him or under his direction and all material and exhibits attached hereto are believed to be true and correct.

This the 27th day of January 2011.

R. Stuart Graham

Affiant

Sworn to and subscribed before me this the 27th day of January 2011

Notary Public, State of Georgia

My Commission Expires: June 16, 2012